A Frame 15 Degree Tilt - Fixing to substructure - F7 Softwood - Using Using 2/Bremick Vortex Universal Screw - 2100 Modules						'	A Frame 1	5 Degree Tilt -		tructure - F al Screw - 2		od - Using Using ules	2/Bremick Vorte	
тс	Roof Pitch	Height	H/d	Zone	SPAN	· · · · · · · · · · · · · · · · · · ·	w	R TC	Roof Pitch	Height	H/d	Zone	SPAN	(mm)
		0≤z≤5m	h/d ≤ 0.5	All	<b>Proline 35</b> 1338	Proline 50 1814				0≤z≤5m	h/d ≤ 0.5	All	<b>Proline 35</b> 1167	1439
			h/d > 0.5 $h/d \le 0.5$	All All	1206 1219	1546 1584					h/d > 0.5 h/d ≤ 0.5	All	1052 1064	1148 1176
	o_	5m <z≤10m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1099</td><td>1262</td><td></td><td></td><td>0_</td><td>5m<z≤10m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>940</td><td>940</td></z≤10m<></td></z≤10m<>	h/d > 0.5	All	1099	1262			0_	5m <z≤10m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>940</td><td>940</td></z≤10m<>	h/d > 0.5	All	940	940
	0≤α<5°	10m <z≤15m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All</td><td>1162 1047</td><td>1426</td><td></td><td></td><td>0≤α&lt;5°</td><td>10m<z≤15m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td>All</td><td>1014 849</td><td>1060 849</td></z≤15m<></td></z≤15m<>	h/d ≤ 0.5 h/d > 0.5	All	1162 1047	1426			0≤α<5°	10m <z≤15m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td>All</td><td>1014 849</td><td>1060 849</td></z≤15m<>	$h/d \le 0.5$ h/d > 0.5	All	1014 849	1060 849
	O NI	15m <z≤20m< td=""><td>h/d ≤ 0.5</td><td>All All</td><td>1130</td><td>1137 1342</td><td></td><td></td><td>O N</td><td>15</td><td><math>h/d \ge 0.5</math></td><td>All</td><td>986</td><td>999</td></z≤20m<>	h/d ≤ 0.5	All All	1130	1137 1342			O N	15	$h/d \ge 0.5$	All	986	999
		15111<2\\\2\\\2\\\10111	h/d > 0.5	All	1019	1071				15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>800</td><td>800</td></z≤20m<>	h/d > 0.5	All	800	800
		20m <z≤30m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All All</td><td>1091 983</td><td>1241 992</td><td></td><td></td><td></td><td>20m<z≤30m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All</td><td>925 742</td><td>925 742</td></z≤30m<></td></z≤30m<>	h/d ≤ 0.5 h/d > 0.5	All All	1091 983	1241 992				20m <z≤30m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All</td><td>925 742</td><td>925 742</td></z≤30m<>	h/d ≤ 0.5 h/d > 0.5	All	925 742	925 742
		0≤z≤5m	h/d ≤ 0.5	All	1338	1814				0≤z≤5m	h/d ≤ 0.5	All	1167	1439
		0=2=0;;;	h/d > 0.5 $h/d \le 0.5$	All All	1206 1219	1546 1584				0-2-0111	h/d > 0.5 h/d ≤ 0.5	All	1052 1064	1148 1176
		5m <z≤10m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1099</td><td>1262</td><td></td><td></td><td>°-</td><td>5m<z≤10m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>940</td><td>940</td></z≤10m<></td></z≤10m<>	h/d > 0.5	All	1099	1262			°-	5m <z≤10m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>940</td><td>940</td></z≤10m<>	h/d > 0.5	All	940	940
C2	5≤α<10°	10m <z≤15m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All</td><td>1162</td><td>1426</td><td></td><td>TC2</td><td>5≤α&lt;10°</td><td>10m<z≤15m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All</td><td>1014</td><td>1060</td></z≤15m<></td></z≤15m<>	h/d ≤ 0.5 h/d > 0.5	All	1162	1426		TC2	5≤α<10°	10m <z≤15m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All</td><td>1014</td><td>1060</td></z≤15m<>	h/d ≤ 0.5 h/d > 0.5	All	1014	1060
2	55(	45	$h/d \ge 0.5$	All All	1047 1130	1137 1342			55C	45	$h/d \ge 0.5$	All	849 986	849 999
		15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1019</td><td>1071</td><td></td><td></td><td>15m<z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>800</td><td>800</td></z≤20m<></td></z≤20m<>	h/d > 0.5	All	1019	1071				15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>800</td><td>800</td></z≤20m<>	h/d > 0.5	All	800	800
		20m <z≤30m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All All</td><td>1091 983</td><td>1241 992</td><td></td><td></td><td></td><td>20m<z≤30m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td>All</td><td>925 742</td><td>925 742</td></z≤30m<></td></z≤30m<>	h/d ≤ 0.5 h/d > 0.5	All All	1091 983	1241 992				20m <z≤30m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td>All</td><td>925 742</td><td>925 742</td></z≤30m<>	$h/d \le 0.5$ h/d > 0.5	All	925 742	925 742
		0≤z≤5m	h/d ≤ 0.5	All	1379	1870				0≤z≤5m	h/d ≤ 0.5	All	1202	1537
			h/d > 0.5 $h/d \le 0.5$	All All	1249 1256	1670 1693					h/d > 0.5 h/d ≤ 0.5	All	1089 1096	1238 1254
	0	5m <z≤10m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1138</td><td>1362</td><td></td><td></td><td>0</td><td>5m<z≤10m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>993</td><td>1013</td></z≤10m<></td></z≤10m<>	h/d > 0.5	All	1138	1362			0	5m <z≤10m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>993</td><td>1013</td></z≤10m<>	h/d > 0.5	All	993	1013
	10≤α≤30	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1197</td><td>1522</td><td></td><td></td><td>10≤α≤30</td><td>10m<z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1045</td><td>1130</td></z≤15m<></td></z≤15m<>	h/d ≤ 0.5	All	1197	1522			10≤α≤30	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1045</td><td>1130</td></z≤15m<>	h/d ≤ 0.5	All	1045	1130
	105	15m == 100	h/d > 0.5 $h/d \le 0.5$	All All	1085 1164	1227 1432			105	1Em == 100	h/d > 0.5 h/d ≤ 0.5	All All	915 1016	915 1065
		15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1055</td><td>1155</td><td></td><td rowspan="2"></td><td></td><td>15m<z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>862</td><td>862</td></z≤20m<></td></z≤20m<>	h/d > 0.5	All	1055	1155				15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>862</td><td>862</td></z≤20m<>	h/d > 0.5	All	862	862
		20m <z≤30m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td>All All</td><td>1124 1018</td><td>1324 1069</td><td></td><td></td><td>20m<z≤30m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All</td><td>980 799</td><td>986 799</td></z≤30m<></td></z≤30m<>	$h/d \le 0.5$ h/d > 0.5	All All	1124 1018	1324 1069				20m <z≤30m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All</td><td>980 799</td><td>986 799</td></z≤30m<>	h/d ≤ 0.5 h/d > 0.5	All	980 799	986 799
		0≤z≤5m	h/d ≤ 0.5	All	1400	1897				0≤z≤5m	h/d ≤ 0.5	All	1220	1586
		0-22-0111	h/d > 0.5 h/d ≤ 0.5	All	1260 1324	1705				0-22-0111	h/d > 0.5 h/d ≤ 0.5	All All	1099	1263
		5m <z≤10m< td=""><td><math>h/d \ge 0.5</math></td><td>All All</td><td>1193</td><td>1795 1510</td><td></td><td></td><td></td><td>5m<z≤10m< td=""><td><math>h/d \ge 0.5</math></td><td>All</td><td>1155 1041</td><td>1406 1121</td></z≤10m<></td></z≤10m<>	$h/d \ge 0.5$	All All	1193	1795 1510				5m <z≤10m< td=""><td><math>h/d \ge 0.5</math></td><td>All</td><td>1155 1041</td><td>1406 1121</td></z≤10m<>	$h/d \ge 0.5$	All	1155 1041	1406 1121
	0≤α<5°	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1256</td><td>1693</td><td></td><td></td><td>0≤α&lt;5°</td><td>10m<z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1096</td><td>1255</td></z≤15m<></td></z≤15m<>	h/d ≤ 0.5	All	1256	1693			0≤α<5°	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1096</td><td>1255</td></z≤15m<>	h/d ≤ 0.5	All	1096	1255
	) VI		h/d > 0.5 $h/d \le 0.5$	All All	1132 1207	1347 1551			) N		h/d > 0.5 h/d ≤ 0.5	All	988 1053	1002 1151
		15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1088</td><td>1235</td><td></td><td></td><td></td><td>15m<z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>921</td><td>921</td></z≤20m<></td></z≤20m<>	h/d > 0.5	All	1088	1235				15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>921</td><td>921</td></z≤20m<>	h/d > 0.5	All	921	921
		20m <z≤30m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All All</td><td>1151 1038</td><td>1397 1114</td><td></td><td></td><td></td><td>20m<z≤30m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td>All</td><td>1005 832</td><td>1039 832</td></z≤30m<></td></z≤30m<>	h/d ≤ 0.5 h/d > 0.5	All All	1151 1038	1397 1114				20m <z≤30m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td>All</td><td>1005 832</td><td>1039 832</td></z≤30m<>	$h/d \le 0.5$ h/d > 0.5	All	1005 832	1039 832
		0≤z≤5m	h/d ≤ 0.5	All	1400	1897				0≤z≤5m	h/d ≤ 0.5	All	1220	1586
		03233111	h/d > 0.5	All	1260	1705				03233111	h/d > 0.5 h/d ≤ 0.5	All	1099	1263
	5≤α<10°	5m <z≤10m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All</td><td>1324 1193</td><td>1795 1510</td><td></td><td><u> </u></td><td>0_</td><td>5m<z≤10m< td=""><td><math>h/d \le 0.5</math></td><td>All</td><td>1155 1041</td><td>1406 1121</td></z≤10m<></td></z≤10m<>	h/d ≤ 0.5 h/d > 0.5	All	1324 1193	1795 1510		<u> </u>	0_	5m <z≤10m< td=""><td><math>h/d \le 0.5</math></td><td>All</td><td>1155 1041</td><td>1406 1121</td></z≤10m<>	$h/d \le 0.5$	All	1155 1041	1406 1121
		10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1256</td><td>1693</td><td></td><td>TC2.5</td><td>Z 10</td><td>10m<z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1096</td><td>1255</td></z≤15m<></td></z≤15m<>	h/d ≤ 0.5	All	1256	1693		TC2.5	Z 10	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1096</td><td>1255</td></z≤15m<>	h/d ≤ 0.5	All	1096	1255
1 D			h/d > 0.5 $h/d \le 0.5$	All	1132 1207	1347 1551	1	2	5≤α<10°		h/d > 0.5 $h/d \le 0.5$	All	988 1053	1002 1151
		15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1088</td><td>1235</td><td></td><td>&gt;</td><td></td><td>15m<z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>921</td><td>921</td></z≤20m<></td></z≤20m<>	h/d > 0.5	All	1088	1235		>		15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>921</td><td>921</td></z≤20m<>	h/d > 0.5	All	921	921
		20m <z≤30m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All</td><td>1151 1038</td><td>1397 1114</td><td></td><td></td><td></td><td>20m<z≤30m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td>All</td><td>1005 832</td><td>1039 832</td></z≤30m<></td></z≤30m<>	h/d ≤ 0.5 h/d > 0.5	All	1151 1038	1397 1114				20m <z≤30m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td>All</td><td>1005 832</td><td>1039 832</td></z≤30m<>	$h/d \le 0.5$ h/d > 0.5	All	1005 832	1039 832
		0≤z≤5m	h/d ≤ 0.5	All	1435	1945				0≤z≤5m	h/d ≤ 0.5	All	1257	1694
		0323011	$h/d > 0.5$ $h/d \le 0.5$	All	1306	1770				0323011	h/d > 0.5 h/d ≤ 0.5	All	1139	1363
	0	5m <z≤10m< td=""><td><math>h/d \ge 0.5</math></td><td>All All</td><td>1364 1235</td><td>1850 1631</td><td></td><td></td><td>0</td><td>5m<z≤10m< td=""><td><math>h/d \ge 0.5</math></td><td>All</td><td>1190 1078</td><td>1501 1210</td></z≤10m<></td></z≤10m<>	$h/d \ge 0.5$	All All	1364 1235	1850 1631			0	5m <z≤10m< td=""><td><math>h/d \ge 0.5</math></td><td>All</td><td>1190 1078</td><td>1501 1210</td></z≤10m<>	$h/d \ge 0.5$	All	1190 1078	1501 1210
	10≤α≤30	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1295</td><td>1755</td><td></td><td></td><td>10≤α≤30</td><td>10m<z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1129</td><td>1339</td></z≤15m<></td></z≤15m<>	h/d ≤ 0.5	All	1295	1755			10≤α≤30	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1129</td><td>1339</td></z≤15m<>	h/d ≤ 0.5	All	1129	1339
	10×		h/d > 0.5 $h/d \le 0.5$	All	1173 1244	1454 1656			10×		h/d > 0.5 $h/d \le 0.5$	All	1023 1085	1081 1228
		15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1127</td><td>1333</td><td></td><td></td><td rowspan="2"></td><td>15m<z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>983</td><td>992</td></z≤20m<></td></z≤20m<>	h/d > 0.5	All	1127	1333				15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>983</td><td>992</td></z≤20m<>	h/d > 0.5	All	983	992
		20m <z≤30m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All All</td><td>1186 1075</td><td>1491 1202</td><td></td><td></td><td>20m<z≤30m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td>All</td><td>1035 896</td><td>1108 896</td></z≤30m<></td></z≤30m<>	h/d ≤ 0.5 h/d > 0.5	All All	1186 1075	1491 1202				20m <z≤30m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td>All</td><td>1035 896</td><td>1108 896</td></z≤30m<>	$h/d \le 0.5$ h/d > 0.5	All	1035 896	1108 896
		0≤z≤5m	$h/d \le 0.5$	All	1467	1988			0≤α<5°	0676Em	$h/d \le 0.5$	All	1278	1732
		05255111	h/d > 0.5	All	1320	1790				0≤z≤5m	h/d > 0.5	All	1151	1397
	_	5m <z≤10m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All</td><td>1467 1320</td><td>1988 1790</td><td></td><td>5m<z≤10m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All</td><td>1278 1151</td><td>1732 1397</td></z≤10m<></td></z≤10m<>	h/d ≤ 0.5 h/d > 0.5	All	1467 1320	1988 1790				5m <z≤10m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All</td><td>1278 1151</td><td>1732 1397</td></z≤10m<>	h/d ≤ 0.5 h/d > 0.5	All	1278 1151	1732 1397
	0≤α<5°	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1368</td><td>1855</td><td></td><td></td><td>10m<z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1193</td><td>1510</td></z≤15m<></td></z≤15m<>	h/d ≤ 0.5	All	1368	1855				10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1193</td><td>1510</td></z≤15m<>	h/d ≤ 0.5	All	1193	1510
	)×		$h/d > 0.5$ $h/d \le 0.5$	All	1232 1296	1622 1757			)¥0		h/d > 0.5 $h/d \le 0.5$	All	1075 1130	1203 1342
		15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1168</td><td>1441</td><td></td><td></td><td></td><td>15m<z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1019</td><td>1071</td></z≤20m<></td></z≤20m<>	h/d > 0.5	All	1168	1441				15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1019</td><td>1071</td></z≤20m<>	h/d > 0.5	All	1019	1071
		20m <z≤30m< td=""><td>h/d &gt; 0.5 h/d &gt; 0.5</td><td>All All</td><td>1219 1099</td><td>1584 1262</td><td></td><td></td><td></td><td>20m<z≤30m< td=""><td>h/d &gt; 0.5 h/d &gt; 0.5</td><td>All All</td><td>1064 940</td><td>1176 940</td></z≤30m<></td></z≤30m<>	h/d > 0.5 h/d > 0.5	All All	1219 1099	1584 1262				20m <z≤30m< td=""><td>h/d &gt; 0.5 h/d &gt; 0.5</td><td>All All</td><td>1064 940</td><td>1176 940</td></z≤30m<>	h/d > 0.5 h/d > 0.5	All All	1064 940	1176 940
		0≤z≤5m	h/d ≤ 0.5	All	1099	1262				0≤z≤5m	$h/d \ge 0.5$ $h/d \le 0.5$	All	1278	1732
		U2Z23III	h/d > 0.5	All	1320	1790				USZSOIII	h/d > 0.5	All	1151	1397
	•	5m <z≤10m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All</td><td>1467 1320</td><td>1988 1790</td><td></td><td></td><td>o_</td><td>5m<z≤10m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td>All</td><td>1278 1151</td><td>1732 1397</td></z≤10m<></td></z≤10m<>	h/d ≤ 0.5 h/d > 0.5	All	1467 1320	1988 1790			o_	5m <z≤10m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td>All</td><td>1278 1151</td><td>1732 1397</td></z≤10m<>	$h/d \le 0.5$ h/d > 0.5	All	1278 1151	1732 1397
C3	5≤α<10°	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1368</td><td>1855</td><td></td><td>S</td><td>5≤α&lt;10°</td><td>10m<z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1193</td><td>1510</td></z≤15m<></td></z≤15m<>	h/d ≤ 0.5	All	1368	1855		S	5≤α<10°	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1193</td><td>1510</td></z≤15m<>	h/d ≤ 0.5	All	1193	1510
2	5≤α		$h/d > 0.5$ $h/d \le 0.5$	All	1232 1296	1622 1757		ľ	5≤α,		h/d > 0.5 $h/d \le 0.5$	All	1075 1130	1203 1342
		15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1168</td><td>1441</td><td></td><td></td><td></td><td>15m<z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1019</td><td>1071</td></z≤20m<></td></z≤20m<>	h/d > 0.5	All	1168	1441				15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1019</td><td>1071</td></z≤20m<>	h/d > 0.5	All	1019	1071
		20m <z≤30m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1219</td><td>1584</td><td></td><td></td><td></td><td>20m<z≤30m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1064</td><td>1176</td></z≤30m<></td></z≤30m<>	h/d > 0.5	All	1219	1584				20m <z≤30m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1064</td><td>1176</td></z≤30m<>	h/d > 0.5	All	1064	1176
			$h/d > 0.5$ $h/d \le 0.5$	All	1099 1485	1262 2013				0//	h/d > 0.5 $h/d \le 0.5$	All	940 1317	940 1785
		0≤z≤5m	h/d > 0.5	All	1368	1854				0≤z≤5m	h/d > 0.5	All	1193	1509
		5m <z≤10m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td>All</td><td>1485 1368</td><td>2013 1854</td><td rowspan="3"></td><td></td><td></td><td>5m<z≤10m< td=""><td><math display="block">h/d \le 0.5</math><math display="block">h/d &gt; 0.5</math></td><td>All</td><td>1317 1193</td><td>1785 1509</td></z≤10m<></td></z≤10m<>	$h/d \le 0.5$ h/d > 0.5	All	1485 1368	2013 1854				5m <z≤10m< td=""><td><math display="block">h/d \le 0.5</math><math display="block">h/d &gt; 0.5</math></td><td>All</td><td>1317 1193</td><td>1785 1509</td></z≤10m<>	$h/d \le 0.5$ $h/d > 0.5$	All	1317 1193	1785 1509
	0≤α≤30	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1410</td><td>1912</td><td></td><td>≤α≤30</td><td>10m<z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1229</td><td>1613</td></z≤15m<></td></z≤15m<>	h/d ≤ 0.5	All	1410	1912			≤α≤30	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1229</td><td>1613</td></z≤15m<>	h/d ≤ 0.5	All	1229	1613
	10≤		h/d > 0.5 h/d ≤ 0.5		1277 1336	1731 1811			10≤α	. 5111 72-2 10111	h/d > 0.5 h/d ≤ 0.5	All	1113	1298
		15m <z≤20m< td=""><td>h/d ≥ 0.5</td><td></td><td>1336 1210</td><td>1811 1557</td><td></td><td></td><td></td><td>15m<z≤20m< td=""><td><math>h/d \le 0.5</math></td><td>All</td><td>1165 1055</td><td>1432 1155</td></z≤20m<></td></z≤20m<>	h/d ≥ 0.5		1336 1210	1811 1557				15m <z≤20m< td=""><td><math>h/d \le 0.5</math></td><td>All</td><td>1165 1055</td><td>1432 1155</td></z≤20m<>	$h/d \le 0.5$	All	1165 1055	1432 1155
		20m <z≤30m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1256</td><td>1693</td><td></td><td></td><td></td><td>20m<z≤30m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1096</td><td>1254</td></z≤30m<></td></z≤30m<>	h/d > 0.5	All	1256	1693				20m <z≤30m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>1096</td><td>1254</td></z≤30m<>	h/d > 0.5	All	1096	1254
			h/d > 0.5	All	1138	1362			1		h/d > 0.5	All	993	1013

WR	тс	Roof Pitch	Height	H/d	Zone	SPAN	(mm)
71 1	16		Tiolynt			Proline 35	Proline 50
			0≤z≤5m	$h/d \le 0.5$	All	1003	1035
				h/d > 0.5 $h/d \le 0.5$	All	829 849	829 849
			5m <z≤10m< td=""><td><math>h/d \ge 0.5</math></td><td>All</td><td>681</td><td>681</td></z≤10m<>	$h/d \ge 0.5$	All	681	681
		ကို		$h/d \ge 0.5$	All	767	767
		0≤α<5°	10m <z≤15m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>616</td><td>616</td></z≤15m<>	h/d > 0.5	All	616	616
		Ö	1E 4- 400	h/d ≤ 0.5	All	723	723
			15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>581</td><td>581</td></z≤20m<>	h/d > 0.5	All	581	581
			20m	h/d ≤ 0.5	All	670	670
			20m <z≤30m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>539</td><td>539</td></z≤30m<>	h/d > 0.5	All	539	539
			0≤z≤5m	h/d ≤ 0.5	All	1003	1035
			USESUII	h/d > 0.5	All	829	829
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>849</td><td>849</td></z≤10m<>	h/d ≤ 0.5	All	849	849
		0 0	5 <u>2</u> _ 10111	h/d > 0.5	All	681	681
	TC2	5≤α<10°	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>767</td><td>767</td></z≤15m<>	h/d ≤ 0.5	All	767	767
	$\vdash$	02.		h/d > 0.5	All	616	616
		"	15m <z≤20m< td=""><td><math>h/d \le 0.5</math></td><td>All</td><td>723 581</td><td>723 591</td></z≤20m<>	$h/d \le 0.5$	All	723 581	723 591
				$h/d > 0.5$ $h/d \le 0.5$	All All	581 670	581 670
			20m <z≤30m< td=""><td><math>h/d \le 0.5</math></td><td>All</td><td>539</td><td>539</td></z≤30m<>	$h/d \le 0.5$	All	539	539
				$h/d \ge 0.5$	All	1033	1104
			0≤z≤5m	h/d > 0.5	All	893	893
			Fm:	h/d ≤ 0.5	All	905	905
			5m <z≤10m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>733</td><td>733</td></z≤10m<>	h/d > 0.5	All	733	733
		Sī	10m/7/15m	h/d ≤ 0.5	All	817	817
		10≤α≤30	10m <z≤15m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>663</td><td>663</td></z≤15m<>	h/d > 0.5	All	663	663
		=	15m <z≤20m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>770</td><td>770</td></z≤20m<>	h/d ≤ 0.5	All	770	770
			1011172320111	h/d > 0.5	All	625	625
			20m <z≤30m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>714</td><td>714</td></z≤30m<>	h/d ≤ 0.5	All	714	714
				h/d > 0.5	All	580	580
			0≤z≤5m	h/d ≤ 0.5	All	1048	1139
				h/d > 0.5	All	911	911
			5m <z≤10m< td=""><td><math display="block">h/d \le 0.5</math><math display="block">h/d &gt; 0.5</math></td><td>All</td><td>992 810</td><td>1011</td></z≤10m<>	$h/d \le 0.5$ $h/d > 0.5$	All	992 810	1011
		ကို		h/d > 0.5 $h/d \le 0.5$	All	810 905	810 905
		0≤α<5°	10m <z≤15m< td=""><td><math>h/d \ge 0.5</math></td><td>All</td><td>905 726</td><td>726</td></z≤15m<>	$h/d \ge 0.5$	All	905 726	726
		%	45 -:	h/d ≤ 0.5	All	831	831
			15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>667</td><td>667</td></z≤20m<>	h/d > 0.5	All	667	667
			20m/=/20	h/d ≤ 0.5	All	752	752
			20m <z≤30m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>604</td><td>604</td></z≤30m<>	h/d > 0.5	All	604	604
			0≤z≤5m	h/d ≤ 0.5	All	1048	1139
			JUZZUIII	h/d > 0.5	All	911	911
ပ	TC2.5	[	5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>992</td><td>1011</td></z≤10m<>	h/d ≤ 0.5	All	992	1011
jior		0 0		h/d > 0.5	All	810	810
Seç		5≤α<10°	10m <z≤15m< td=""><td><math>h/d \le 0.5</math></td><td>All</td><td>905</td><td>905</td></z≤15m<>	$h/d \le 0.5$	All	905	905
J Di		\( \) \( \) \( \) \( \)		h/d > 0.5 h/d ≤ 0.5	All	726	726
Wind Region C		"	15m <z≤20m< td=""><td><math>h/d \le 0.5</math></td><td>All</td><td>831 667</td><td>831 667</td></z≤20m<>	$h/d \le 0.5$	All	831 667	831 667
_				$h/d \ge 0.5$	All	752	752
			20m <z≤30m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>604</td><td>604</td></z≤30m<>	h/d > 0.5	All	604	604
			0/7/5	h/d ≤ 0.5	All	1080	1214
			0≤z≤5m	h/d > 0.5	All	978	982
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1022</td><td>1078</td></z≤10m<>	h/d ≤ 0.5	All	1022	1078
		98	5m -2=10m	h/d > 0.5	All	873	873
		10≤α≤30	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>964</td><td>964</td></z≤15m<>	h/d ≤ 0.5	All	964	964
		0 0		h/d > 0.5	All	781	781
		-	15m <z≤20m< td=""><td><math>h/d \le 0.5</math></td><td>All</td><td>886</td><td>886</td></z≤20m<>	$h/d \le 0.5$	All	886	886
				h/d > 0.5	All	718	718
			20m <z≤30m< td=""><td><math display="block">h/d \le 0.5</math><math display="block">h/d &gt; 0.5</math></td><td>All</td><td>801 650</td><td>801 650</td></z≤30m<>	$h/d \le 0.5$ $h/d > 0.5$	All	801 650	801 650
				$h/d \ge 0.5$	All	1098	1259
			0≤z≤5m	$h/d \ge 0.5$	All	989	1006
			Fm:110	h/d ≤ 0.5	All	1098	1259
			5m <z≤10m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>989</td><td>1006</td></z≤10m<>	h/d > 0.5	All	989	1006
		\ \doc{\doc{\doc{\doc{\doc{\doc{\doc{	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1025</td><td>1085</td></z≤15m<>	h/d ≤ 0.5	All	1025	1085
		0≤α<5°	10111-2>15111	h/d > 0.5	All	868	868
			15m <z≤20m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>967</td><td>967</td></z≤20m<>	h/d ≤ 0.5	All	967	967
			10.111 -Z=ZUIII	h/d > 0.5	All	775	775
			20m <z≤30m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>849</td><td>849</td></z≤30m<>	h/d > 0.5	All	849	849
				h/d > 0.5	All	681	681
			0≤z≤5m	$h/d \le 0.5$	All	1098	1259
				h/d > 0.5	All	989	1006
	TC3		5m <z≤10m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All</td><td>1098 989</td><td>1259 1006</td></z≤10m<>	h/d ≤ 0.5 h/d > 0.5	All	1098 989	1259 1006
		10°		$h/d \ge 0.5$	All	1025	1085
		5≤α<10°	10m <z≤15m< td=""><td><math>h/d \ge 0.5</math></td><td>All</td><td>868</td><td>868</td></z≤15m<>	$h/d \ge 0.5$	All	868	868
		55	45	h/d ≤ 0.5	All	967	967
			15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>775</td><td>775</td></z≤20m<>	h/d > 0.5	All	775	775
			20m <z≤30m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>849</td><td>849</td></z≤30m<>	h/d > 0.5	All	849	849
			ZUII1~Z>3UIII	h/d > 0.5	All	681	681
			0≤z≤5m	h/d ≤ 0.5	All	1131	1343
			JUZZUIII	h/d > 0.5	All	1025	1084
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1131</td><td>1343</td></z≤10m<>	h/d ≤ 0.5	All	1131	1343
		30		h/d > 0.5	All	1025	1084
		0≤α≤30	10m <z≤15m< td=""><td><math>h/d \le 0.5</math></td><td>All</td><td>1056</td><td>1157</td></z≤15m<>	$h/d \le 0.5$	All	1056	1157
		105		h/d > 0.5	All	936	936
		,	15m <z≤20m< td=""><td><math display="block">h/d \le 0.5</math><math display="block">h/d &gt; 0.5</math></td><td>All All</td><td>1001 834</td><td>1030 834</td></z≤20m<>	$h/d \le 0.5$ $h/d > 0.5$	All All	1001 834	1030 834
				h/d > 0.5	All	905	905
		1	20m <z≤30m< td=""><td> 0.0</td><td>/30</td><td>555</td><td>300</td></z≤30m<>	0.0	/30	555	300

WR	тс	Roof Pitch	Height	H/d	Zone	SPAN	(mm)	DESIGN FARAIVETERS
WK	10	ROOT I ILCH	rieigni			Proline 35	Proline 50	WIND PARAMETERS ARE IN ACCORDANCE WITH AS/NZS1170.2:20
			0≤z≤5m	$h/d \le 0.5$ $h/d > 0.5$		731	731 587	TABLES ARE SUITABLE FOR BUILDINGS INCLUSIVE OF PARAMETE
				$h/d \ge 0.5$		587 601	601	
		0≤α<5°	5m <z≤10m< td=""><td>h/d &gt; 0.5</td><td></td><td>484</td><td>484</td><td>ASSUMPTION MANUAL ATTACHED.</td></z≤10m<>	h/d > 0.5		484	484	ASSUMPTION MANUAL ATTACHED.
			10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td></td><td>544</td><td>544</td><td>REGION = A, B, C, D Base Wind Speed</td></z≤15m<>	h/d ≤ 0.5		544	544	REGION = A, B, C, D Base Wind Speed
			10111<2515111	h/d > 0.5		438	438	IMPORTANCE LEVEL = 2
			15m <z≤20m< td=""><td>h/d ≤ 0.5</td><td></td><td>513</td><td>513</td><td>DESIGN LIFE = 25 YEARS Region A B</td></z≤20m<>	h/d ≤ 0.5		513	513	DESIGN LIFE = 25 YEARS Region A B
				h/d > 0.5 $h/d \le 0.5$		413	413	ANNUAL PROBABILITY = $1/200$ Vr(m/s) 43 52 6
			20m <z≤30m< td=""><td><math>h/d \ge 0.5</math></td><td></td><td>476 383</td><td>476 383</td><td>VI(III/3)   43   32   0</td></z≤30m<>	$h/d \ge 0.5$		476 383	476 383	VI(III/3)   43   32   0
			0.1.15	h/d ≤ 0.5		731	731	CENEDAL
			0≤z≤5m	h/d > 0.5		587	587	GENERAL CONTRACTOR CON
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td></td><td>601</td><td>601</td><td><ul><li>SPAN TABLE TO BE READ WITH PARTRIDGE ASSUMPTIONS</li></ul></td></z≤10m<>	h/d ≤ 0.5		601	601	<ul><li>SPAN TABLE TO BE READ WITH PARTRIDGE ASSUMPTIONS</li></ul>
		°0		h/d > 0.5		484	484	<ul> <li>REVIEW OF SUPPORTING BUILDING FOR STRUCTURAL AD</li> </ul>
	TC2	5≤α<10°	10m <z≤15m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td></td><td>544 438</td><td>544 438</td><td><ul> <li>REVIEW OF ROOF SHEETING FOR STRUCTURAL ADEQUAC</li> </ul></td></z≤15m<>	$h/d \le 0.5$ h/d > 0.5		544 438	544 438	<ul> <li>REVIEW OF ROOF SHEETING FOR STRUCTURAL ADEQUAC</li> </ul>
	'		45	h/d ≤ 0.5		513	513	THESE SPANS ARE ONLY APPLICABLE TO CONTINUOUS R
			15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td></td><td>413</td><td>413</td><td>BELOW FOR SPAN REDUCTION FACTORS FOR RAILS SUPI</td></z≤20m<>	h/d > 0.5		413	413	BELOW FOR SPAN REDUCTION FACTORS FOR RAILS SUPI
			20m <z≤30m< td=""><td>h/d ≤ 0.5</td><td></td><td>476</td><td>476</td><td>REVIEW OF SOLAR PANEL STRUCTURAL CAPACITY BY OT</td></z≤30m<>	h/d ≤ 0.5		476	476	REVIEW OF SOLAR PANEL STRUCTURAL CAPACITY BY OT
			20 2-00	h/d > 0.5		383	383	A-FRAMES TO BE FIXED TO THE SUB STRUCTURE OR ROO
		10≤α≤30	0≤z≤5m	$h/d \le 0.5$ h/d > 0.5		779 632	779 632	NOTED IN THE TABLE.
				h/d ≤ 0.5		640	640	
			5m <z≤10m< td=""><td>h/d &gt; 0.5</td><td></td><td>520</td><td>520</td><td>ALL FIXTURES TO BE INSTALLED TO THE MANUFACTURER</td></z≤10m<>	h/d > 0.5		520	520	ALL FIXTURES TO BE INSTALLED TO THE MANUFACTURER
			10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td></td><td>579</td><td>579</td><td>ALLOWANCE HAS BEEN MADE FOR A SOLAR PANEL SELF \</td></z≤15m<>	h/d ≤ 0.5		579	579	ALLOWANCE HAS BEEN MADE FOR A SOLAR PANEL SELF \
			10111 32=10111	h/d > 0.5		471	471	<ul> <li>2 RAILS MINIMUM ARE TO BE USED FOR ALL WIND REGION</li> </ul>
			15m <z≤20m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td></td><td>546</td><td>546</td><td>LENGTH FROM THE EDGE.</td></z≤20m<>	h/d ≤ 0.5 h/d > 0.5		546	546	LENGTH FROM THE EDGE.
				$h/d \ge 0.5$		444 507	444 507	PANELS TO BE ORIENTATED IN THE PORTRAIT POSITION.
			20m <z≤30m< td=""><td>h/d &gt; 0.5</td><td></td><td>412</td><td>412</td><td><ul> <li>ALL RAILS ARE TO BE JOINED WITH RAIL CONNECTORS DO</li> </ul></td></z≤30m<>	h/d > 0.5		412	412	<ul> <li>ALL RAILS ARE TO BE JOINED WITH RAIL CONNECTORS DO</li> </ul>
			0≤z≤5m	h/d ≤ 0.5		803	803	Z-14.4-639.
		ညှိ	05253111	h/d > 0.5		645	645	ALL RAILS TO SPAN THREE FULL SPAN MINIMUM (BE SUPP
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td></td><td>715</td><td>715</td><td>MAXIMUM OF 40% OF THE ADJACENT SPAN CAPACITY.</td></z≤10m<>	h/d ≤ 0.5		715	715	MAXIMUM OF 40% OF THE ADJACENT SPAN CAPACITY.
				h/d > 0.5 $h/d \le 0.5$		574 640	574	
		0≤α<5°	10m <z≤15m< td=""><td><math>h/d \ge 0.5</math></td><td></td><td>515</td><td>640 515</td><td>ALL RAILS, CLAMPS AND FASTENERS TO BE INSTALLED IN</td></z≤15m<>	$h/d \ge 0.5$		515	640 515	ALL RAILS, CLAMPS AND FASTENERS TO BE INSTALLED IN
		ŏ	45	h/d ≤ 0.5		589	589	DOCUMENTATION.
			15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td></td><td>474</td><td>474</td><td><ul> <li>FASTENERS FIXED TO TIMBER MUST HAVE AN EDGE DISTA</li> </ul></td></z≤20m<>	h/d > 0.5		474	474	<ul> <li>FASTENERS FIXED TO TIMBER MUST HAVE AN EDGE DISTA</li> </ul>
			20m <z≤30m< td=""><td>h/d ≤ 0.5</td><td></td><td>533</td><td>533</td><td>THIS IS IN COMPLIANCE WITH EDGE DISTANCES OUTLINED</td></z≤30m<>	h/d ≤ 0.5		533	533	THIS IS IN COMPLIANCE WITH EDGE DISTANCES OUTLINED
				h/d > 0.5		429	429	$_{\perp}$ $ullet$ FASTENERS FIXED TO TIMBER FRAMING MUST USE A BREI
			0≤z≤5m	$h/d \le 0.5$ h/d > 0.5	All	803 645	803 645	DIAMETER OF 6.2mm, AND A MINIMUM EMBEDMENT OF 35n
				h/d ≤ 0.5		715	715	→ TIMBER PURLINS MUST HAVE A MINIMUM WIDTH OF 10D W
		5≤α<10°	5m <z≤10m< td=""><td>h/d &gt; 0.5</td><td></td><td>574</td><td>574</td><td>• TIMBER PURLINS MUST HAVE A MINIMUM GRADE OF F7 AS</td></z≤10m<>	h/d > 0.5		574	574	• TIMBER PURLINS MUST HAVE A MINIMUM GRADE OF F7 AS
Wind Region	C2.5		10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td></td><td>640</td><td>640</td><td>FASTENERS FIXED TO COLD FORMED STEEL PURLINS MUST</td></z≤15m<>	h/d ≤ 0.5		640	640	FASTENERS FIXED TO COLD FORMED STEEL PURLINS MUST
	2			h/d > 0.5		515	515	DIAMETER OF THE SCREW. THIS IS IN COMPLIANCE WITH I
۸in			15m <z≤20m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td></td><td>589 474</td><td>589 474</td><td>STEEL PURLINS MUST HAVE A MINIMUM BASE METAL EQU.</td></z≤20m<>	$h/d \le 0.5$ h/d > 0.5		589 474	589 474	STEEL PURLINS MUST HAVE A MINIMUM BASE METAL EQU.
-			00 100	h/d ≤ 0.5	All	533	533	STEEL PURLINS MUST HAVE A MINIMUM WITDTH OF 6D WH
			20m <z≤30m< td=""><td>h/d &gt; 0.5</td><td></td><td>429</td><td>429</td><td>PARTRIDGE ENGINEERS Pty Ltd PREPARED DOCUMENTATION</td></z≤30m<>	h/d > 0.5		429	429	PARTRIDGE ENGINEERS Pty Ltd PREPARED DOCUMENTATION
			0≤z≤5m	h/d ≤ 0.5	All	856	856	
				h/d > 0.5 $h/d \le 0.5$		694	694	USE BY SCHLETTER AUSTRALIA PTY LTD ONLY.
		10≤α≤30	5m <z≤10m< td=""><td><math>h/d \ge 0.5</math></td><td>All</td><td>761 618</td><td>761 618</td><td><ul> <li>INSTALLATION VERIFICATION AND ASSOCIATED CERTIFICATION</li> </ul></td></z≤10m<>	$h/d \ge 0.5$	All	761 618	761 618	<ul> <li>INSTALLATION VERIFICATION AND ASSOCIATED CERTIFICATION</li> </ul>
			10 115	h/d ≤ 0.5		682	682	$\dashv$ $ullet$ NO ALLOWANCE HAS BEEN MADE FOR HYDRAULIC, HAIL C
		]≥α	10m <z≤15m< td=""><td>h/d &gt; 0.5</td><td></td><td>554</td><td>554</td><td><ul> <li>INSTALLATION OUTSIDE THE SPECIFIC PARAMETERS REQ</li> </ul></td></z≤15m<>	h/d > 0.5		554	554	<ul> <li>INSTALLATION OUTSIDE THE SPECIFIC PARAMETERS REQ</li> </ul>
		)1	15m <z≤20m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>627</td><td>627</td><td><ul><li>INSTALLATIONS IN TERRAIN CATEGORY = 1.0, REDUCE EQ</li></ul></td></z≤20m<>	h/d ≤ 0.5	All	627	627	<ul><li>INSTALLATIONS IN TERRAIN CATEGORY = 1.0, REDUCE EQ</li></ul>
			10111 32=20111	h/d > 0.5		510	510	FOLLOWING;
			20m <z≤30m< td=""><td>h/d ≤ 0.5 h/d &gt; 0.5</td><td>All</td><td>568 462</td><td>568 462</td><td>Region A = 18%</td></z≤30m<>	h/d ≤ 0.5 h/d > 0.5	All	568 462	568 462	Region A = 18%
				h/d ≤ 0.5	All	886	886	Region B = 18%
		°C	0≤z≤5m	h/d > 0.5		711	711	Region C/D = Specific engineering review required.
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td></td><td>886</td><td>886</td><td>REFER TO AS1170.2:2021 SECTION 4.2.1 FOR THE DETERM</td></z≤10m<>	h/d ≤ 0.5		886	886	REFER TO AS1170.2:2021 SECTION 4.2.1 FOR THE DETERM
			0 2_10	h/d > 0.5		711	711	SOLAR PANELS HAVE BEEN CHECKED FOR WIND LOADING
		0≤α<5°	10m <z≤15m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td>All</td><td>766 615</td><td>766 615</td><td></td></z≤15m<>	$h/d \le 0.5$ h/d > 0.5	All	766 615	766 615	
		0	45	$h/d \le 0.5$		684	684	FOR THE VARIOUS SPANS AND WIND REGIONS.
			15m <z≤20m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>549</td><td>549</td><td>• ALL SPANS IN THE TABLE MUST BE MULTIPLIED BY A RED</td></z≤20m<>	h/d > 0.5	All	549	549	• ALL SPANS IN THE TABLE MUST BE MULTIPLIED BY A RED
			20m <z≤30m< td=""><td>h/d &gt; 0.5</td><td></td><td>601</td><td>601</td><td>ROOF.</td></z≤30m<>	h/d > 0.5		601	601	ROOF.
			20111 - 2220111	h/d > 0.5		484	484	REDUCTION FACTORS FOR RAILS S
			0≤z≤5m	$h/d \le 0.5$ h/d > 0.5		886	886	REDUCTION FACTORS FOR RAILS S
				$h/d \le 0.5$		711 886	711 886	FASTENERS
		5≤¤<10°	5m <z≤10m< td=""><td>h/d &gt; 0.5</td><td></td><td>711</td><td>711</td><td>TAGILITE</td></z≤10m<>	h/d > 0.5		711	711	TAGILITE
	TC3		10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td></td><td>766</td><td>766</td><td>ODANO EDOM THE ADOME TARKE CANINGT RE HOER ON CONTINU</td></z≤15m<>	h/d ≤ 0.5		766	766	ODANO EDOM THE ADOME TARKE CANINGT RE HOER ON CONTINU
			1011112210111	h/d > 0.5	All	615	615	SPANS FROM THE ABOVE TABLE CANNOT BE USED ON CONTINU
			15m <z≤20m< td=""><td><math>h/d \le 0.5</math> h/d &gt; 0.5</td><td>All</td><td>684</td><td>684</td><td>THAN 4 A-FRAMES. WHERE A RAIL IS SUPPORTED BY LESS THAN</td></z≤20m<>	$h/d \le 0.5$ h/d > 0.5	All	684	684	THAN 4 A-FRAMES. WHERE A RAIL IS SUPPORTED BY LESS THAN
				h/d > 0.5	All	549 601	549 601	SHOULD BE MULTIPLIED BY THE BELOW FACTOR.
			20m <z≤30m< td=""><td>h/d &gt; 0.5</td><td>All</td><td>484</td><td>484</td><td>DAIL OURDORT REPUICTION FACTOR 0.00</td></z≤30m<>	h/d > 0.5	All	484	484	DAIL OURDORT REPUICTION FACTOR 0.00
			0≤z≤5m	h/d ≤ 0.5	All	944	944	RAIL SUPPORT REDUCTION FACTOR = 0.89
			USZSIII	h/d > 0.5	All	765	765	NOTE: DAIL MUST SDAN DETWEEN MAN TWO FASTENEDS
			5m <z≤10m< td=""><td><math>h/d \le 0.5</math></td><td>All</td><td>944</td><td>944</td><td>NOTE: RAIL MUST SPAN BETWEEN MIN TWO FASTENERS.</td></z≤10m<>	$h/d \le 0.5$	All	944	944	NOTE: RAIL MUST SPAN BETWEEN MIN TWO FASTENERS.
		230		h/d > 0.5 $h/d \le 0.5$	All	765 816	765 816	-
		10≤α≤30	10m <z≤15m< td=""><td><math>h/d \le 0.5</math></td><td></td><td>816 662</td><td>816 662</td><td>-</td></z≤15m<>	$h/d \le 0.5$		816 662	816 662	-
		10	15m <z≤20m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>728</td><td>728</td><td></td></z≤20m<>	h/d ≤ 0.5	All	728	728	
			15111-2-20111	h/d > 0.5	All	591	591	
			20m <z≤30m< td=""><td>h/d &gt; 0.5</td><td></td><td>640</td><td>640</td><td>-</td></z≤30m<>	h/d > 0.5		640	640	-
		<u> </u>	<u> </u>	h/d > 0.5	All	520	520	

A Frame 15 Degree Tilt - Fixing to substructure - F7 Softwood - Using Using 2/Bremick Vortex

Universal Screw - 2100 Modules

## **DESIGN PARAMETERS**

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WIND PARAMETERS ARE IN ACCORDANCE WITH AS/NZS1170.2:2021. EARTHQUAKE AND SNOW LOADS ARE EXCLUDED TABLES ARE SUITABLE FOR BUILDINGS INCLUSIVE OF PARAMETERS REFFERED TO IN THE TABLES BELOW AND ASSUMPTION MANUAL ATTACHED.

Region | A | B | C | D Vr(m/s) | 43 | 52 | 61 | 72

#### **GENERAL**

SPAN TABLE TO BE READ WITH PARTRIDGE ASSUMPTIONS MANUAL

- REVIEW OF SUPPORTING BUILDING FOR STRUCTURAL ADEQUACY TO SUPPORT PANEL INSTALLATION BY OTHERS.
- REVIEW OF ROOF SHEETING FOR STRUCTURAL ADEQUACY TO SUPPORT PANEL INSALLATION BY OTHERS.
- THESE SPANS ARE ONLY APPLICABLE TO CONTINUOUS RAILS SUPPORTED BY A MINIMUM OF 4 A-FRAMES. SEE BELOW FOR SPAN REDUCTION FACTORS FOR RAILS SUPPORTED BY LESS THAN 4 A-FRAMES.
- REVIEW OF SOLAR PANEL STRUCTURAL CAPACITY BY OTHERS.
- A-FRAMES TO BE FIXED TO THE SUB STRUCTURE OR ROOF SHEETING WITH THE QUANTITY AND TYPE OF SCREWS NOTED IN THE TABLE.
- ALL FIXTURES TO BE INSTALLED TO THE MANUFACTURERS SPECIFICATIONS.
- ALLOWANCE HAS BEEN MADE FOR A SOLAR PANEL SELF WEIGHT OF 0.15 kPa.
- 2 RAILS MINIMUM ARE TO BE USED FOR ALL WIND REGIONS. RAILS TO BE LOCATED 15%-25% OF THE PANELS
- LENGTH FROM THE EDGE.
- ALL RAILS ARE TO BE JOINED WITH RAIL CONNECTORS DOCUMENTED IN SCHLETTER Pty Ltd TECHNICAL ARTICLE
- ALL RAILS TO SPAN THREE FULL SPAN MINIMUM (BE SUPPORTED BY MIN 4 FASTENERS). CANTILEVERS TO BE A
- MAXIMUM OF 40% OF THE ADJACENT SPAN CAPACITY. • ALL RAILS, CLAMPS AND FASTENERS TO BE INSTALLED IN ACCORDANCE WITH THEIR RELEVANT SCHLETTER INC.
- DOCUMENTATION. • FASTENERS FIXED TO TIMBER MUST HAVE AN EDGE DISTANCE OF 5D, WHERE 'D' IS THE DIAMETER OF THE SCREW.
- THIS IS IN COMPLIANCE WITH EDGE DISTANCES OUTLINED IN AS1720.1:2010 SECTION 4.3.4.
- FASTENERS FIXED TO TIMBER FRAMING MUST USE A BREMICK VORTEX UNIVERSAL SCREW, WITH MINIMUM
- DIAMETER OF 6.2mm, AND A MINIMUM EMBEDMENT OF 35mm. TIMBER PURLINS MUST HAVE A MINIMUM WIDTH OF 10D WHERE D IS THE DIAMETER OF THE TIMBER SCREW.
- TIMBER PURLINS MUST HAVE A MINIMUM GRADE OF F7 AS DEFINED IN AS1720.1.
- FASTENERS FIXED TO COLD FORMED STEEL PURLINS MUST HAVE AN EDGE DISTANCE OF 3D WHERE 'D' IS THE DIAMETER OF THE SCREW. THIS IS IN COMPLIANCE WITH EDGE DISTANCES OUTLINED IN AS4600:2-18 SECTION 5.4.3
- STEEL PURLINS MUST HAVE A MINIMUM BASE METAL EQUAL TO THE VALUE SPECIFIED IN THE TABLE.
- STEEL PURLINS MUST HAVE A MINIMUM WITDTH OF 6D WHERE D IS THE DIAMETER OF THE STEEL SCREW.
- PARTRIDGE ENGINEERS Pty Ltd PREPARED DOCUMENTATION, PROJECT NUMBER 2021S0925, IS FOR THE EXCLUSIVE
- USE BY SCHLETTER AUSTRALIA PTY LTD ONLY.
- INSTALLATION VERIFICATION AND ASSOCIATED CERTIFICATION IS BY OTHERS. • NO ALLOWANCE HAS BEEN MADE FOR HYDRAULIC, HAIL OR SNOW LOADING.
- INSTALLATION OUTSIDE THE SPECIFIC PARAMETERS REQUIRES SPECIFIC ENGINEERING ANALYSIS.
- INSTALLATIONS IN TERRAIN CATEGORY = 1.0, REDUCE EQUIVALENT TERRAIN CATEGORY 2.0 VALUES BY THE
- FOLLOWING; Region A = 18%
- Region B = 18%
- Region C/D = Specific engineering review required.
- REFER TO AS1170.2:2021 SECTION 4.2.1 FOR THE DETERMINATION OF TERRAIN CATEGORY.
- SOLAR PANELS HAVE BEEN CHECKED FOR WIND LOADINGS AND SHOULD BE CERTIFIED BY THE MANUFACTURER
- FOR THE VARIOUS SPANS AND WIND REGIONS.
- ALL SPANS IN THE TABLE MUST BE MULTIPLIED BY A REDUCTION FACTOR BASED ON THEIR POSITION ON THE

## **REDUCTION FACTORS FOR RAILS SUPPORTED BY LESS THAN 4 FASTENERS**

SPANS FROM THE ABOVE TABLE CANNOT BE USED ON CONTINUOUS RAILS THAT ARE SUPPORTED BY LESS THAN 4 A-FRAMES. WHERE A RAIL IS SUPPORTED BY LESS THAN 4 A-FRAMES THE SPANS IN THE TABLE SHOULD BE MULTIPLIED BY THE BELOW FACTOR.

# ROOF

ALL A-FRAME SPACINGS IN THE ABOVE TABLE MUST BE MULTIPLIED BY ONE OF THE BELOW FACTORS BASED ON THEIR LOCATION ON THE ROOF.

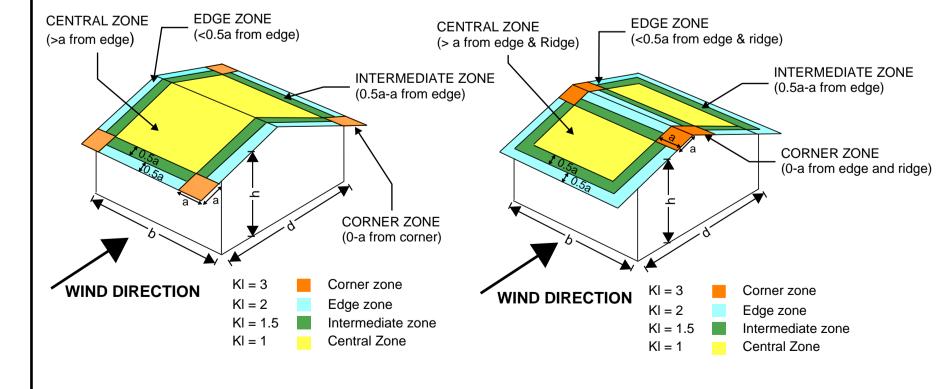
CORNER ZONE: SPACINGS MUST BE MULTIPLIED BY 0.33

EDGE ZONE: SPACINGS MUST BE MULTIPLIED BY 0.5

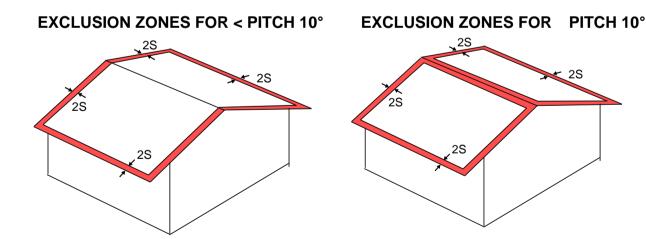
INTERMEDIATE ZONE: SPACINGS MUST BE MULTIPLIED BY 0.66 CENTRAL ZONE: SPACINGS DO NOT NEED TO BE MULTIPLIED BY ANY FACTOR

#### WHERE a = MIN(0.2d, 0.2b) if h/d or h/b 0.2, or 2h if h/d and h/b < 0.2

ROOF ZONES FOR ROOVES WITH PITCHES < 10° ROOF ZONE FOR ROOVES WITH PITCHES 10°



#### NEL EXCLUSION ZONE & MOUNTING RESTRAINTS



PANELS MUST NOT BE INSTALLED WITHIN A DISTANCE OF 2S FROM THE ROOF EDGE WHERE S IS THE GAP BETWEEN THE UNDERSIDE OF THE PANEL AND THE ROOF SURFACE (ROOF EDGE INCLUDES RIDGES WITH

THE EXCLUSION ZONE SHOWN ABOVE MUST BE MIN 200mm.

THE GAP BETWEEN THE UNDERSIDE OF THE PANEL AND THE ROOF SURFACE MUST BE MIN 50mm AND MAX 300mm

## **TERRAIN CATEGORY DEFINITIONS**

AS1170.2 :2021 CLAUSE 4.2.1

TC1 - VERY EXPOSED OPEN TERRAIN WITH VERY FEW OR NO OBSTRUCTIONS, AND ALL WATER SURFACES

TC2 - OPEN TERRAIN, INCLUDING GRASSLAND, WITH WELL SCATTER OBSTRUCTIONS HAVING HEIGHTS GENERALLY FROM 1.5m TO 5m, WITH NO MORE THAN TWO OBSTRUCTIONS PER HECTARE

TC2.5 - TERRAIN WITH SOME TREES OR ISOLATED OBSTRUCTIONS, TERRAIN IN DEVELOPING OUTER URBAN AREAS WITH SCATTERED HOUSES, OR LARGE ACREAGE DEVELOPMENTS WITH MORE THAN TWO AND LESS THAN 10 BUILDINGS PER HECTARE

TC3 - TERRAIN WITH NUMEROUS CLOSELY SPACED OBSTRUCTIONS HAVING HEIGHTS GENERALLY FROM 3m TO 10m. THE MINIMUM DENSITY OF OBSTRUCTIONS SHALL BE ATLEAST THE EQUIVALENT OF 10 HOUSE-SIZE OBSTRUCTIONS PER HECTARE

TC4 - TERRAIN WITH NUMEROUS LARGE, HIGH (10m TO 30m TALL) AND CLOSELY SPACED CONSTRUCTIONS, SUCH AS LARGE CITY CENTRES AND WELL-DEVELOPED INDUSTRIAL COMPELXES.

## ALTERATIONS TO SPAN TABLES FOR **SOLAR PANEL SIZE**

THIS SPAN TABLE IS FOR SOLAR PANELS OF SIZE 2100x1100mm, EACH RAIL SUPPORTS A SOLAR PANEL WIDTH OF 1050mm. THE SPACINGS SHOWN IN THE TABLES HAVE BEEN CALCULATED ASSUMING EACH PANEL IS SUPPORTED WITH TWO RAILS. THE SPANS IN THE TABLE CAN BE ALTERED FOR LARGER & SMALLER SOLAR PANELS USING THE FOLLOWING EQUATIONS.

FOR SOLAR PANELS WITH WIDTH LARGER THAN 2100mm

$$Span * \frac{2100}{y}$$

Where y = NEW SOLAR PANEL WIDTH IN mm

FOR SOLAR PANELS WITH WIDTH SMALLER THAN 2100mm

$$Span * \sqrt{\frac{2100}{y}}$$

WHERE y = NEW SOLAR PANEL WIDTH IN mm

## **ALTERATIONS TO SPAN TABLES FOR ADDITIONAL RAILS**

THIS SPAN TABLE IS FOR SOLAR PANELS OF SIZE 2100x1100mm. EACH RAIL SUPPORTS A SOLAR PANEL WIDTH OF 1050mm. THE SPACINGS SHOWN IN THE TABLES HAVE BEEN CALCULATED ASSUMING EACH PANEL IS SUPPORTED WITH TWO RAILS. THE SPANS IN THE TABLE CAN BE ALTERED FOR ADDITIONAL RAILS USING THE FOLLOWING EQUATION.

$$Span * \sqrt{\frac{1050}{\left(\frac{2100}{n}\right)^2}}$$

WHERE n = THE TOTAL NUMBER RAILS SUPPORTING THE PANEL. RAILS MUST BE SPACED SO THAT

THEY SUPPORT EVEN WIDTHS OF THE PANEL.

Rev.	Issue / Amendment	Ву	App.	Date	

JW AKD 4/10/2023



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SCHLETTER AUSTRALIA PTY LTD

A FOR INFORMATION

2021S0925

A FRAME 15 DEGREE SETUP FIXING TO F7 SOFTWOOD USING 2/BREMICK VOTREX UNIVERSAL SCREWS

2100 MODULES

2021S0925

ELECTRONIC SIGNATURE: THIS DRAWING HAS BEEN ASSIGNED AN ELECTRONIC SIGNATURE DO NOT SCALE DRAWINGS CODE. THE PRESENCE OF THIS CODE SIGNIFIES THAT THIS IS THE USE FIGURED DIMENSIONS CERTIFIED DRAWING ISSUED FOR CONSTRUCTION. Electronic Code Signature Date Designed JW Scale at A1 Drawn 04/10/2023 JW Job No. Drawing No. Revision