			al Screw - 2			d (mm)		I			al Screw -			N (mm)
R TO	Roof Pitch	Height	H/d	Zone	SPAI Proline 35	N (mm) Proline 50	WR	TC	Roof Pitch	Height	H/d	Zone	Proline 35	N (mm) Proline 50
		0≤z≤5m	h/d ≤ 0.5 h/d > 0.5		1101 1111	1429 1457			0≤α<5°	0≤z≤5m	h/d ≤ 0.5 h/d > 0.5		962 970	1065 1085
		5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1005</td><td>1169</td><td></td><td></td><td>5m<z≤10m< td=""><td>h/d ≤ 0.</td><td>5 All</td><td>874</td><td>874</td></z≤10m<></td></z≤10m<>	h/d ≤ 0.5	All	1005	1169				5m <z≤10m< td=""><td>h/d ≤ 0.</td><td>5 All</td><td>874</td><td>874</td></z≤10m<>	h/d ≤ 0.	5 All	874	874
	2°		h/d > 0.5 $h/d \le 0.5$		1013 958	1192 1055					h/d > 0.: h/d ≤ 0.:		885 789	890 789
	0≤α<5°	10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>966</td><td>1075</td><td></td><td rowspan="8">TC2</td><td>10m<z≤15m< td=""><td>h/d > 0.</td><td></td><td>804</td><td>804</td></z≤15m<></td></z≤15m<>	h/d > 0.5	All	966	1075		TC2		10m <z≤15m< td=""><td>h/d > 0.</td><td></td><td>804</td><td>804</td></z≤15m<>	h/d > 0.		804	804
	0	15m <z≤20m< td=""><td>h/d ≤ 0.5 h/d > 0.5</td><td>All</td><td>932</td><td>994</td><td rowspan="5"></td><td>15m<z≤20m< td=""><td>h/d ≤ 0.5 h/d > 0.5</td><td></td><td>744</td><td>744</td></z≤20m<></td></z≤20m<>	h/d ≤ 0.5 h/d > 0.5	All	932	994				15m <z≤20m< td=""><td>h/d ≤ 0.5 h/d > 0.5</td><td></td><td>744</td><td>744</td></z≤20m<>	h/d ≤ 0.5 h/d > 0.5		744	744
		00 4 400	$h/d \ge 0.5$	All	940 899	1013 921				20 4 420	h/d ≤ 0.		758 690	758 690
		20m <z≤30m< td=""><td>h/d > 0.5</td><td></td><td>907</td><td>939</td><td></td><td>20m<z≤30m< td=""><td>h/d > 0.</td><td>5 All</td><td>703</td><td>703</td></z≤30m<></td></z≤30m<>	h/d > 0.5		907	939				20m <z≤30m< td=""><td>h/d > 0.</td><td>5 All</td><td>703</td><td>703</td></z≤30m<>	h/d > 0.	5 All	703	703
		0≤z≤5m	h/d ≤ 0.5 h/d > 0.5	All	1101 1111	1429 1457			5≤α<10°	0≤z≤5m	h/d ≤ 0.: h/d > 0.:		962 970	1065 1085
		5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1005</td><td>1169</td><td>5m<z≤10m< td=""><td>h/d ≤ 0.</td><td>5 All</td><td>874</td><td>874</td></z≤10m<></td></z≤10m<>	h/d ≤ 0.5	All	1005	1169				5m <z≤10m< td=""><td>h/d ≤ 0.</td><td>5 All</td><td>874</td><td>874</td></z≤10m<>	h/d ≤ 0.	5 All	874	874
	.01		h/d > 0.5 h/d ≤ 0.5	All	1013 958	1192 1055					h/d > 0.9 h/d ≤ 0.9		885 789	890 789
1C2	5≤α<10°	10m <z≤15m< td=""><td>h/d > 0.5</td><td></td><td>966</td><td>1075</td><td rowspan="7"></td><td>10m<z≤15m< td=""><td>h/d > 0.</td><td>5 All</td><td>804</td><td>804</td></z≤15m<></td></z≤15m<>	h/d > 0.5		966	1075				10m <z≤15m< td=""><td>h/d > 0.</td><td>5 All</td><td>804</td><td>804</td></z≤15m<>	h/d > 0.	5 All	804	804
	22	15m <z≤20m< td=""><td>$h/d \le 0.5$$h/d > 0.5$</td><td>All</td><td>932 940</td><td>994 1013</td><td></td><td>2</td><td>15m<z≤20m< td=""><td>$h/d \le 0.5$ h/d > 0.5</td><td></td><td>744 758</td><td>744 758</td></z≤20m<></td></z≤20m<>	$h/d \le 0.5$ $h/d > 0.5$	All	932 940	994 1013			2	15m <z≤20m< td=""><td>$h/d \le 0.5$ h/d > 0.5</td><td></td><td>744 758</td><td>744 758</td></z≤20m<>	$h/d \le 0.5$ h/d > 0.5		744 758	744 758
		20m <z≤30m< td=""><td>$h/d \ge 0.5$</td><td>All</td><td>899</td><td>921</td><td></td><td rowspan="9">10≤α≤30</td><td>20m<z≤30m< td=""><td>h/d ≤ 0.</td><td></td><td>690</td><td>690</td></z≤30m<></td></z≤30m<>	$h/d \ge 0.5$	All	899	921			10≤α≤30	20m <z≤30m< td=""><td>h/d ≤ 0.</td><td></td><td>690</td><td>690</td></z≤30m<>	h/d ≤ 0.		690	690
		20m<2≤30m	h/d > 0.5	All	907	939				20m<2≤30m	h/d > 0.		703	703
		0≤z≤5m	$h/d \le 0.5$ h/d > 0.5		1024 1050	1220 1288				0≤z≤5m	h/d ≤ 0.: h/d > 0.:		895 917	911 961
		5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>934</td><td>1000</td><td></td><td>5m<z≤10m< td=""><td>h/d ≤ 0.</td><td>5 All</td><td>749</td><td>749</td></z≤10m<></td></z≤10m<>	h/d ≤ 0.5	All	934	1000				5m <z≤10m< td=""><td>h/d ≤ 0.</td><td>5 All</td><td>749</td><td>749</td></z≤10m<>	h/d ≤ 0.	5 All	749	749
	230		h/d > 0.5 $h/d \le 0.5$	All	958 891	1055 903					h/d > 0.5 $h/d \le 0.5$		789 677	789 677
	10≤α≤30	10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>913</td><td>952</td><td></td><td></td><td>10m<z≤15m< td=""><td>h/d > 0.</td><td>5 All</td><td>713</td><td>713</td></z≤15m<></td></z≤15m<>	h/d > 0.5	All	913	952				10m <z≤15m< td=""><td>h/d > 0.</td><td>5 All</td><td>713</td><td>713</td></z≤15m<>	h/d > 0.	5 All	713	713
	_	15m <z≤20m< td=""><td>h/d ≤ 0.5 h/d > 0.5</td><td>All All</td><td>851 889</td><td>851 898</td><td></td><td></td><td>15m<z≤20m< td=""><td>h/d ≤ 0.: h/d > 0.:</td><td></td><td>638 673</td><td>638 673</td></z≤20m<></td></z≤20m<>	h/d ≤ 0.5 h/d > 0.5	All All	851 889	851 898				15m <z≤20m< td=""><td>h/d ≤ 0.: h/d > 0.:</td><td></td><td>638 673</td><td>638 673</td></z≤20m<>	h/d ≤ 0.: h/d > 0.:		638 673	638 673
		20m/7/20	$h/d \ge 0.5$ $h/d \le 0.5$		789	789				20m/3/20-	h/d ≤ 0.	5 All	592	592
		20m <z≤30m< td=""><td>h/d > 0.5</td><td>All</td><td>832</td><td>832</td><td></td><td></td><td>20m<z≤30m< td=""><td>h/d > 0.</td><td>5 All</td><td>624</td><td>624</td></z≤30m<></td></z≤30m<>	h/d > 0.5	All	832	832				20m <z≤30m< td=""><td>h/d > 0.</td><td>5 All</td><td>624</td><td>624</td></z≤30m<>	h/d > 0.	5 All	624	624
		0≤z≤5m	$h/d \le 0.5$ h/d > 0.5	All	1151 1161	1560 1574			0≤α<5°	0≤z≤5m	$h/d \le 0.5$ h/d > 0.5		1005 1014	1170 1193
		5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1090</td><td>1396</td><td></td><td rowspan="2"></td><td>5m<z≤10m< td=""><td>h/d ≤ 0.</td><td>5 All</td><td>952</td><td>1040</td></z≤10m<></td></z≤10m<>	h/d ≤ 0.5	All	1090	1396				5m <z≤10m< td=""><td>h/d ≤ 0.</td><td>5 All</td><td>952</td><td>1040</td></z≤10m<>	h/d ≤ 0.	5 All	952	1040
	0≤α<5°		h/d > 0.5 $h/d \le 0.5$		1099 1035	1423 1247					h/d > 0. $h/d \le 0.$		960 904	1060 931
		10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>1044</td><td>1271</td><td></td><td></td><td>10m<z≤15m< td=""><td>h/d > 0.</td><td>5 All</td><td>912</td><td>949</td></z≤15m<></td></z≤15m<>	h/d > 0.5	All	1044	1271				10m <z≤15m< td=""><td>h/d > 0.</td><td>5 All</td><td>912</td><td>949</td></z≤15m<>	h/d > 0.	5 All	912	949
		15m <z≤20m< td=""><td>$h/d \le 0.5$ h/d > 0.5</td><td>All All</td><td>995 1004</td><td>1145 1167</td><td></td><td rowspan="7">TC2.5</td><td>15m<z≤20m< td=""><td>h/d ≤ 0.: h/d > 0.:</td><td></td><td>856 872</td><td>856 872</td></z≤20m<></td></z≤20m<>	$h/d \le 0.5$ h/d > 0.5	All All	995 1004	1145 1167		TC2.5		15m <z≤20m< td=""><td>h/d ≤ 0.: h/d > 0.:</td><td></td><td>856 872</td><td>856 872</td></z≤20m<>	h/d ≤ 0.: h/d > 0.:		856 872	856 872
		20m <z≤30m< td=""><td>h/d ≤ 0.5</td><td></td><td>949</td><td>1034</td><td rowspan="11">Wind Region B</td><td>20m<z≤30m< td=""><td>h/d ≤ 0.</td><td>_</td><td>774</td><td>774</td></z≤30m<></td></z≤30m<>	h/d ≤ 0.5		949	1034	Wind Region B			20m <z≤30m< td=""><td>h/d ≤ 0.</td><td>_</td><td>774</td><td>774</td></z≤30m<>	h/d ≤ 0.	_	774	774
		2011-2230111	h/d > 0.5		957	1054				2011 - 2 30111	h/d > 0.5		788	788
		0≤z≤5m	$h/d \le 0.5$ $h/d > 0.5$	All	1151 1161	1560 1574			5≤α<10°	0≤z≤5m	$h/d \le 0.5$ h/d > 0.5	_	1005 1014	1170 1193
		5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1090</td><td>1396</td><td>5m<z≤10m< td=""><td>h/d ≤ 0.</td><td></td><td>952</td><td>1040</td></z≤10m<></td></z≤10m<>	h/d ≤ 0.5	All	1090	1396				5m <z≤10m< td=""><td>h/d ≤ 0.</td><td></td><td>952</td><td>1040</td></z≤10m<>	h/d ≤ 0.		952	1040
TC2 5	.10°	10	h/d > 0.5 $h/d \le 0.5$	All	1099 1035	1423 1247				10	h/d > 0. $h/d \le 0.$		960 904	1060 931
[]	5≤α<10°	10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>1044</td><td>1271</td><td>10m<z≤15m< td=""><td>h/d > 0.</td><td>5 All</td><td>912</td><td>949</td></z≤15m<></td></z≤15m<>	h/d > 0.5	All	1044	1271				10m <z≤15m< td=""><td>h/d > 0.</td><td>5 All</td><td>912</td><td>949</td></z≤15m<>	h/d > 0.	5 All	912	949
	Ψ	15m <z≤20m< td=""><td>$h/d \le 0.5$ h/d > 0.5</td><td>All</td><td>995 1004</td><td>1145 1167</td><td></td><td>Ŋ</td><td>15m<z≤20m< td=""><td>$h/d \le 0.5$ h/d > 0.5</td><td></td><td>856 872</td><td>856 872</td></z≤20m<></td></z≤20m<>	$h/d \le 0.5$ h/d > 0.5	All	995 1004	1145 1167			Ŋ	15m <z≤20m< td=""><td>$h/d \le 0.5$ h/d > 0.5</td><td></td><td>856 872</td><td>856 872</td></z≤20m<>	$h/d \le 0.5$ h/d > 0.5		856 872	856 872
		20m <z≤30m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>949</td><td>1034</td><td rowspan="6"></td><td></td><td>20m<z≤30m< td=""><td>h/d ≤ 0.</td><td></td><td>774</td><td>774</td></z≤30m<></td></z≤30m<>	h/d ≤ 0.5	All	949	1034				20m <z≤30m< td=""><td>h/d ≤ 0.</td><td></td><td>774</td><td>774</td></z≤30m<>	h/d ≤ 0.		774	774
		2011-230111	h/d > 0.5	All	957	1054			10≤α≤30	2011-230111	h/d > 0.5 $h/d \le 0.5$	_	788	788
		0≤z≤5m	$h/d \le 0.5$ h/d > 0.5	All	1070 1097	1342 1418				0≤z≤5m	h/d > 0.	5 All	935 958	1001 1056
	10≤α≤30	5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1014</td><td>1192</td><td>5m<z≤10m< td=""><td>h/d ≤ 0.</td><td></td><td>885</td><td>891</td></z≤10m<></td></z≤10m<>	h/d ≤ 0.5	All	1014	1192				5m <z≤10m< td=""><td>h/d ≤ 0.</td><td></td><td>885</td><td>891</td></z≤10m<>	h/d ≤ 0.		885	891
		10 115	h/d > 0.5 $h/d \le 0.5$	All	1039 963	1259 1066				10 115	h/d > 0. $h/d \le 0.$		908 798	939 798
		10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>987</td><td>1125</td><td></td><td>10m<z≤15m< td=""><td>h/d > 0.</td><td>5 All</td><td>841</td><td>841</td></z≤15m<></td></z≤15m<>	h/d > 0.5	All	987	1125				10m <z≤15m< td=""><td>h/d > 0.</td><td>5 All</td><td>841</td><td>841</td></z≤15m<>	h/d > 0.	5 All	841	841
	_	15m <z≤20m< td=""><td>$h/d \le 0.5$ h/d > 0.5</td><td>All</td><td>925 949</td><td>979 1033</td><td></td><td></td><td>~</td><td>15m<z≤20m< td=""><td>h/d ≤ 0.: h/d > 0.:</td><td></td><td>733 773</td><td>733 773</td></z≤20m<></td></z≤20m<>	$h/d \le 0.5$ h/d > 0.5	All	925 949	979 1033			~	15m <z≤20m< td=""><td>h/d ≤ 0.: h/d > 0.:</td><td></td><td>733 773</td><td>733 773</td></z≤20m<>	h/d ≤ 0.: h/d > 0.:		733 773	733 773
		20m <z≤30m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>883</td><td>885</td><td></td><td rowspan="3"></td><td rowspan="6">0sa<5°</td><td>20m<z≤30m< td=""><td>h/d ≤ 0.</td><td>5 All</td><td>664</td><td>664</td></z≤30m<></td></z≤30m<>	h/d ≤ 0.5	All	883	885			0sa<5°	20m <z≤30m< td=""><td>h/d ≤ 0.</td><td>5 All</td><td>664</td><td>664</td></z≤30m<>	h/d ≤ 0.	5 All	664	664
			h/d > 0.5 h/d ≤ 0.5		905	934				20111 -Z=30111	h/d > 0.5 h/d ≤ 0.5		700 1052	700
		0≤z≤5m	$h/d \le 0.5$	All	1205 1216	1634 1648				0≤z≤5m	h/d ≤ 0.5		1052 1062	1293 1318
		5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1205</td><td>1634</td><td>, </td><td></td><td>5m<z≤10m< td=""><td>h/d ≤ 0.</td><td>5 All</td><td>1052</td><td>1293</td></z≤10m<></td></z≤10m<>	h/d ≤ 0.5	All	1205	1634	,			5m <z≤10m< td=""><td>h/d ≤ 0.</td><td>5 All</td><td>1052</td><td>1293</td></z≤10m<>	h/d ≤ 0.	5 All	1052	1293
	<5°	10	h/d > 0.5 $h/d \le 0.5$	All	1216 1126	1648 1499				10	h/d > 0.5 $h/d \le 0.5$	5 All	1062 983	1318 1116
	0≤α<5°	10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>1136</td><td>1528</td><td></td><td></td><td>10m<z≤15m< td=""><td>h/d > 0.</td><td>5 All</td><td>992</td><td>1137</td></z≤15m<></td></z≤15m<>	h/d > 0.5	All	1136	1528				10m <z≤15m< td=""><td>h/d > 0.</td><td>5 All</td><td>992</td><td>1137</td></z≤15m<>	h/d > 0.	5 All	992	1137
		15m <z≤20m< td=""><td>$h/d \le 0.5$ h/d > 0.5</td><td>All</td><td>1067 1076</td><td>1333 1359</td><td></td><td></td><td>-</td><td>15m<z≤20m< td=""><td>$h/d \le 0.5$ h/d > 0.5</td><td>_</td><td>932 940</td><td>994</td></z≤20m<></td></z≤20m<>	$h/d \le 0.5$ h/d > 0.5	All	1067 1076	1333 1359			-	15m <z≤20m< td=""><td>$h/d \le 0.5$ h/d > 0.5</td><td>_</td><td>932 940</td><td>994</td></z≤20m<>	$h/d \le 0.5$ h/d > 0.5	_	932 940	994
		20m <z≤30m< td=""><td>h/d > 0.5</td><td>All</td><td>1005</td><td>1169</td><td></td><td></td><td></td><td>20m<z≤30m< td=""><td>h/d > 0.</td><td>5 All</td><td>874</td><td>874</td></z≤30m<></td></z≤30m<>	h/d > 0.5	All	1005	1169				20m <z≤30m< td=""><td>h/d > 0.</td><td>5 All</td><td>874</td><td>874</td></z≤30m<>	h/d > 0.	5 All	874	874
			h/d > 0.5 $h/d \le 0.5$	All All	1013 1205	1192 1634			5≤α<10°		h/d > 0. $h/d \le 0.$		885 1052	890 1293
		0≤z≤5m	h/d > 0.5	All	1216	1648				0≤z≤5m	h/d > 0.5		1062	1318
		5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1205</td><td>1634</td><td></td><td></td><td>5m<z≤10m< td=""><td>h/d ≤ 0.5</td><td>5 All</td><td>1052</td><td>1293</td></z≤10m<></td></z≤10m<>	h/d ≤ 0.5	All	1205	1634				5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>5 All</td><td>1052</td><td>1293</td></z≤10m<>	h/d ≤ 0.5	5 All	1052	1293
63	:10°		h/d > 0.5 $h/d \le 0.5$	All	1216 1126	1648 1499		ŭ			h/d > 0. $h/d \le 0.$		1062 983	1318 1116
133	5≤α<10°	10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>1136</td><td>1528</td><td></td><td>753</td><td>10m<z≤15m< td=""><td>h/d > 0.</td><td>5 All</td><td>992</td><td>1137</td></z≤15m<></td></z≤15m<>	h/d > 0.5	All	1136	1528		753		10m <z≤15m< td=""><td>h/d > 0.</td><td>5 All</td><td>992</td><td>1137</td></z≤15m<>	h/d > 0.	5 All	992	1137
	Ω	15m <z≤20m< td=""><td>$h/d \le 0.5$$h/d > 0.5$</td><td>All</td><td>1067 1076</td><td>1333 1359</td><td></td><td></td><td>ω</td><td>15m<z≤20m< td=""><td>h/d ≤ 0.: h/d > 0.:</td><td></td><td>932 940</td><td>994</td></z≤20m<></td></z≤20m<>	$h/d \le 0.5$ $h/d > 0.5$	All	1067 1076	1333 1359			ω	15m <z≤20m< td=""><td>h/d ≤ 0.: h/d > 0.:</td><td></td><td>932 940</td><td>994</td></z≤20m<>	h/d ≤ 0.: h/d > 0.:		932 940	994
		20m <z≤30m< td=""><td>h/d > 0.5</td><td></td><td>1005</td><td>1169</td><td></td><td rowspan="5"></td><td></td><td>20m<z≤30m< td=""><td>h/d > 0.</td><td>5 All</td><td>874</td><td>874</td></z≤30m<></td></z≤30m<>	h/d > 0.5		1005	1169				20m <z≤30m< td=""><td>h/d > 0.</td><td>5 All</td><td>874</td><td>874</td></z≤30m<>	h/d > 0.	5 All	874	874
			h/d > 0.5 h/d ≤ 0.5	All	1013	1192			10≤α≤30		h/d > 0.: h/d ≤ 0.:	_	885	890
		0≤z≤5m	$h/d \le 0.5$	All	1121 1149	1485 1558				0≤z≤5m	h/d ≤ 0.5		979 1003	1105 1167
		5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>1121</td><td>1485</td><td>5m<z≤10m< td=""><td>h/d ≤ 0.</td><td>All</td><td>979</td><td>1105</td></z≤10m<></td></z≤10m<>	h/d ≤ 0.5	All	1121	1485				5m <z≤10m< td=""><td>h/d ≤ 0.</td><td>All</td><td>979</td><td>1105</td></z≤10m<>	h/d ≤ 0.	All	979	1105
	<30		h/d > 0.5 $h/d \le 0.5$	All	1149 1047	1558 1279					h/d > 0. $h/d \le 0.$		1003 914	1167 954
	10≤α≤30	10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>1073</td><td>1351</td><td></td><td>10m<z≤15m< td=""><td>h/d > 0.</td><td>5 All</td><td>937</td><td>1007</td></z≤15m<></td></z≤15m<>	h/d > 0.5	All	1073	1351				10m <z≤15m< td=""><td>h/d > 0.</td><td>5 All</td><td>937</td><td>1007</td></z≤15m<>	h/d > 0.	5 All	937	1007
	=	15m <z≤20m< td=""><td>h/d ≤ 0.5 h/d > 0.5</td><td></td><td>993</td><td>1139</td><td></td><td rowspan="3"></td><td>15m<z≤20m< td=""><td>h/d ≤ 0.5 h/d > 0.5</td><td></td><td>851 880</td><td>851</td></z≤20m<></td></z≤20m<>	h/d ≤ 0.5 h/d > 0.5		993	1139				15m <z≤20m< td=""><td>h/d ≤ 0.5 h/d > 0.5</td><td></td><td>851 880</td><td>851</td></z≤20m<>	h/d ≤ 0.5 h/d > 0.5		851 880	851
		20m/=/20	h/d > 0.5	All	1018 934	1202 1000	-			20m/=/20=	h/d > 0.5		889 749	898 749
		20m <z≤30m< td=""><td>h/d > 0.5</td><td></td><td>958</td><td>1055</td><td>20m<z≤30m< td=""><td>h/d > 0.</td><td></td><td>789</td><td>789</td></z≤30m<></td></z≤30m<>	h/d > 0.5		958	1055				20m <z≤30m< td=""><td>h/d > 0.</td><td></td><td>789</td><td>789</td></z≤30m<>	h/d > 0.		789	789

WR	TC	Roof Pitch	Height	H/d	2100 Mc	SPAN	
••••				h/d ≤ 0.5	All	Proline 35	Proline 50
			0≤z≤5m	h/d > 0.5	All	771 786	771 786
			En- 4- 440	h/d ≤ 0.5	All	634	634
			5m <z≤10m< td=""><td>h/d > 0.5</td><td>All</td><td>646</td><td>646</td></z≤10m<>	h/d > 0.5	All	646	646
		0≤α<5°	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>574</td><td>574</td></z≤15m<>	h/d ≤ 0.5	All	574	574
) so	10111-2=10111	h/d > 0.5	All	584	584
			15m <z≤20m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>541</td><td>541</td></z≤20m<>	h/d ≤ 0.5	All	541	541
				h/d > 0.5	All	551	551
			20m <z≤30m< td=""><td>$h/d \le 0.5$$h/d > 0.5$</td><td>All All</td><td>502 512</td><td>502 512</td></z≤30m<>	$h/d \le 0.5$ $h/d > 0.5$	All All	502 512	502 512
				h/d ≤ 0.5	All	771	771
			0≤z≤5m	h/d > 0.5	All	786	786
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>634</td><td>634</td></z≤10m<>	h/d ≤ 0.5	All	634	634
		°C	5111~2≤10111	h/d > 0.5	All	646	646
	TC2	5≤α<10°	10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>574</td><td>574</td></z≤15m<>	h/d ≤ 0.5	All	574	574
	Η	250		h/d > 0.5 h/d ≤ 0.5	All	584	584
			15m <z≤20m< td=""><td>$h/d \ge 0.5$</td><td>All All</td><td>541 551</td><td>541 551</td></z≤20m<>	$h/d \ge 0.5$	All All	541 551	541 551
			00 100	h/d ≤ 0.5	All	502	502
			20m <z≤30m< td=""><td>h/d > 0.5</td><td>All</td><td>512</td><td>512</td></z≤30m<>	h/d > 0.5	All	512	512
			0≤z≤5m	h/d ≤ 0.5	All	661	661
			ひっとうり	h/d > 0.5	All	697	697
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>544</td><td>544</td></z≤10m<>	h/d ≤ 0.5	All	544	544
		99		h/d > 0.5	All	574	574
		10≤α≤30	10m <z≤15m< td=""><td>$h/d \le 0.5$$h/d > 0.5$</td><td>All All</td><td>493 519</td><td>493 519</td></z≤15m<>	$h/d \le 0.5$ $h/d > 0.5$	All All	493 519	493 519
		10;		$h/d \ge 0.5$	All	465	465
			15m <z≤20m< td=""><td>h/d > 0.5</td><td>All</td><td>490</td><td>490</td></z≤20m<>	h/d > 0.5	All	490	490
			20m <z≤30m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>432</td><td>432</td></z≤30m<>	h/d ≤ 0.5	All	432	432
			∠∪111~Z≥3UM	h/d > 0.5	All	455	455
			0≤z≤5m	h/d ≤ 0.5	All	847	847
				h/d > 0.5	All	863	863
			5m <z≤10m< td=""><td>$h/d \le 0.5$$h/d > 0.5$</td><td>All All</td><td>754 768</td><td>754</td></z≤10m<>	$h/d \le 0.5$ $h/d > 0.5$	All All	754 768	754
		ညှိ		$h/d \ge 0.5$	All	675	768 675
		0≤α<5°	10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>688</td><td>688</td></z≤15m<>	h/d > 0.5	All	688	688
			45	h/d ≤ 0.5	All	621	621
			15m <z≤20m< td=""><td>h/d > 0.5</td><td>All</td><td>633</td><td>633</td></z≤20m<>	h/d > 0.5	All	633	633
			20m <z≤30m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>563</td><td>563</td></z≤30m<>	h/d ≤ 0.5	All	563	563
			2011 -2=00111	h/d > 0.5	All	573	573
		5≤α<10°	0≤z≤5m	h/d ≤ 0.5	All	847	847
				$h/d > 0.5$ $h/d \le 0.5$	All All	863 754	863 754
Wind Region C			5m <z≤10m< td=""><td>h/d > 0.5</td><td>All</td><td>768</td><td>768</td></z≤10m<>	h/d > 0.5	All	768	768
èg	TC2.5		10m <z≤15m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>675</td><td>675</td></z≤15m<>	h/d ≤ 0.5	All	675	675
R.	7		10111<2515111	h/d > 0.5	All	688	688
/jii			15m <z≤20m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>621</td><td>621</td></z≤20m<>	h/d ≤ 0.5	All	621	621
>				$h/d > 0.5$ $h/d \le 0.5$	All	633	633
			20m <z≤30m< td=""><td>$h/d \ge 0.5$</td><td>All All</td><td>563 573</td><td>563 573</td></z≤30m<>	$h/d \ge 0.5$	All All	563 573	563 573
			0.1.15	h/d ≤ 0.5	All	726	726
			0≤z≤5m	h/d > 0.5	All	765	765
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>646</td><td>646</td></z≤10m<>	h/d ≤ 0.5	All	646	646
		30	0111 -22 - 10111	h/d > 0.5	All	681	681
		10sas30	10m <z≤15m< td=""><td>$h/d \le 0.5$</td><td>All</td><td>580</td><td>580</td></z≤15m<>	$h/d \le 0.5$	All	580	580
		10≤		$h/d > 0.5$ $h/d \le 0.5$	All All	611 533	611 533
			15m <z≤20m< td=""><td>$h/d \ge 0.5$</td><td>All</td><td>562</td><td>533</td></z≤20m<>	$h/d \ge 0.5$	All	562	533
			20	h/d ≤ 0.5	All	483	483
-			20m <z≤30m< td=""><td>h/d > 0.5</td><td>All</td><td>509</td><td>509</td></z≤30m<>	h/d > 0.5	All	509	509
			0≤z≤5m	h/d ≤ 0.5	All	905	934
		0≤α<5°	JUZZUIII	h/d > 0.5	All	913	952
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>905</td><td>934</td></z≤10m<>	h/d ≤ 0.5	All	905	934
				$h/d > 0.5$ $h/d \le 0.5$	All	913	952
			10m <z≤15m< td=""><td>$h/d \le 0.5$$h/d > 0.5$</td><td>All All</td><td>807 823</td><td>807 823</td></z≤15m<>	$h/d \le 0.5$ $h/d > 0.5$	All All	807 823	807 823
				$h/d \ge 0.5$	All	721	721
			15m <z≤20m< td=""><td>h/d > 0.5</td><td>All</td><td>734</td><td>734</td></z≤20m<>	h/d > 0.5	All	734	734
			20m <z≤30m< td=""><td>h/d > 0.5</td><td>All</td><td>634</td><td>634</td></z≤30m<>	h/d > 0.5	All	634	634
			ZUIIINZSJUM	h/d > 0.5	All	646	646
			0≤z≤5m	h/d ≤ 0.5	All	905	934
				h/d > 0.5	All	913	952
			5m <z≤10m< td=""><td>$h/d \le 0.5$ h/d > 0.5</td><td>All</td><td>905</td><td>934</td></z≤10m<>	$h/d \le 0.5$ h/d > 0.5	All	905	934
	8	10。		$h/d > 0.5$ $h/d \le 0.5$	All All	913 807	952 807
	TC3	5≤α<10°	10m <z≤15m< td=""><td>$h/d \ge 0.5$</td><td>All</td><td>823</td><td>823</td></z≤15m<>	$h/d \ge 0.5$	All	823	823
	•	55	15m /=/00	h/d ≤ 0.5	All	721	721
			15m <z≤20m< td=""><td>h/d > 0.5</td><td>All</td><td>734</td><td>734</td></z≤20m<>	h/d > 0.5	All	734	734
			20m <z≤30m< td=""><td>h/d > 0.5</td><td>All</td><td>634</td><td>634</td></z≤30m<>	h/d > 0.5	All	634	634
			2011 -Z=30111	h/d > 0.5	All	646	646
			0≤z≤5m	h/d ≤ 0.5	All	800	800
				$h/d > 0.5$ $h/d \le 0.5$	All	844	844
			5m <z≤10m< td=""><td>$h/d \le 0.5$</td><td>All All</td><td>800 844</td><td>800 844</td></z≤10m<>	$h/d \le 0.5$	All All	800 844	800 844
		58	40	h/d ≤ 0.5	All	692	692
		10≤α≤30	10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>730</td><td>730</td></z≤15m<>	h/d > 0.5	All	730	730
		+	15m <z≤20m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>618</td><td>618</td></z≤20m<>	h/d ≤ 0.5	All	618	618
			1011174240111	h/d > 0.5	All	652	652
- 1		1	20m <z≤30m< td=""><td>h/d > 0.5</td><td>All</td><td>544</td><td>544</td></z≤30m<>	h/d > 0.5	All	544	544

	то.	Poof Ditch		sal Screw - 21		SPAN	(mm)	DESIGN PARAME			
WR	TC	Roof Pitch	Height	H/d	Zone	Proline 35	Proline 50	WIND PARAMETERS ARE IN ACC			
			0≤z≤5m	h/d ≤ 0.5 h/d > 0.5	All	547 558	547 558	TABLES ARE SUITABLE FOR BUI			
		0≤α<5°	5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>451</td><td>451</td><td>ASSUMPTION MANUAL ATTACHE</td></z≤10m<>	h/d ≤ 0.5	All	451	451	ASSUMPTION MANUAL ATTACHE			
				h/d > 0.5 h/d ≤ 0.5	All	460 408	460 408	REGION = A, B, C, D			
			10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>416</td><td>416</td><td>IMPORTANCE LEVEL = 2</td></z≤15m<>	h/d > 0.5	All	416	416	IMPORTANCE LEVEL = 2			
			15m <z≤20m< td=""><td>h/d ≤ 0.5 h/d > 0.5</td><td>All</td><td>386 393</td><td>386 393</td><td>DESIGN LIFE = 25 YEARS</td></z≤20m<>	h/d ≤ 0.5 h/d > 0.5	All	386 393	386 393	DESIGN LIFE = 25 YEARS			
			20m <z≤30m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>358</td><td>358</td><td>ANNUAL PROBABILITY = 1/200</td></z≤30m<>	h/d ≤ 0.5	All	358	358	ANNUAL PROBABILITY = 1/200			
			20111~2≦30111	h/d > 0.5	All	365	365				
			0≤z≤5m	h/d ≤ 0.5 h/d > 0.5	All	547 558	547 558	GENERAL			
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>451</td><td>451</td><td>SPAN TABLE TO BE READ W</td></z≤10m<>	h/d ≤ 0.5	All	451	451	SPAN TABLE TO BE READ W			
	TC2	5≤α<10°		h/d > 0.5 h/d ≤ 0.5	All	460 408	460 408	REVIEW OF SUPPORTING BY			
			10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>416</td><td>416</td><td>REVIEW OF ROOF SHEETING</td></z≤15m<>	h/d > 0.5	All	416	416	REVIEW OF ROOF SHEETING			
			15m <z≤20m< td=""><td>h/d ≤ 0.5 h/d > 0.5</td><td>All</td><td>386 393</td><td>386 393</td><td>THESE SPANS ARE ONLY A</td></z≤20m<>	h/d ≤ 0.5 h/d > 0.5	All	386 393	386 393	THESE SPANS ARE ONLY A			
			20m <z≤30m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>358</td><td>358</td><td>BELOW FOR SPAN REDUCT</td></z≤30m<>	h/d ≤ 0.5	All	358	358	BELOW FOR SPAN REDUCT			
			2011-23011	h/d > 0.5 h/d ≤ 0.5	All	365	365	REVIEW OF SOLAR PANEL S			
		10≤α≤30	0≤z≤5m	h/d ≥ 0.5	All	470 495	470 495	A-FRAMES TO BE FIXED TO			
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>388</td><td>388</td><td> NOTED IN THE TABLE. ALL FIXTURES TO BE INSTA </td></z≤10m<>	h/d ≤ 0.5	All	388	388	 NOTED IN THE TABLE. ALL FIXTURES TO BE INSTA 			
			10	h/d > 0.5 h/d ≤ 0.5	All	408 351	408 351	ALLOWANCE HAS BEEN MAI			
			10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>370</td><td>370</td><td>2 RAILS MINIMUM ARE TO BI</td></z≤15m<>	h/d > 0.5	All	370	370	2 RAILS MINIMUM ARE TO BI			
			15m <z≤20m< td=""><td>h/d ≤ 0.5 h/d > 0.5</td><td>All</td><td>331 349</td><td>331 349</td><td>LENGTH FROM THE EDGE.</td></z≤20m<>	h/d ≤ 0.5 h/d > 0.5	All	331 349	331 349	LENGTH FROM THE EDGE.			
			20m <z≤30m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>308</td><td>308</td><td>PANELS TO BE ORIENTATED</td></z≤30m<>	h/d ≤ 0.5	All	308	308	PANELS TO BE ORIENTATED			
			20111~2≤30111	h/d > 0.5	All	324	324	• ALL RAILS ARE TO BE JOINE			
	TC2.5	0≤α<5°	0≤z≤5m	h/d ≤ 0.5 h/d > 0.5	All	601 612	601 612	Z-14.4-639.			
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>535</td><td>535</td><td>ALL RAILS TO SPAN THREE</td></z≤10m<>	h/d ≤ 0.5	All	535	535	ALL RAILS TO SPAN THREE			
				h/d > 0.5 h/d ≤ 0.5	All	545 480	545 480	MAXIMUM OF 40% OF THE A			
			10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>489</td><td>489</td><td>ALL RAILS, CLAMPS AND FA</td></z≤15m<>	h/d > 0.5	All	489	489	ALL RAILS, CLAMPS AND FA			
			15m <z≤20m< td=""><td>h/d ≤ 0.5 h/d > 0.5</td><td>All</td><td>442</td><td>442</td><td>DOCUMENTATION.</td></z≤20m<>	h/d ≤ 0.5 h/d > 0.5	All	442	442	DOCUMENTATION.			
			2000 4742000	h/d ≤ 0.5	All	450 401	450 401	FASTENERS FIXED TO TIMB THIS IS IN COMPLIANCE WITH			
			20m <z≤30m< td=""><td>h/d > 0.5</td><td>All</td><td>408</td><td>408</td><td> THIS IS IN COMPLIANCE WIT FASTENERS FIXED TO TIMB </td></z≤30m<>	h/d > 0.5	All	408	408	 THIS IS IN COMPLIANCE WIT FASTENERS FIXED TO TIMB 			
		5≤α<10°	0≤z≤5m	h/d ≤ 0.5 h/d > 0.5	All	601 612	601 612	DIAMETER OF 6.2mm, AND A			
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>535</td><td>535</td><td>TIMBER PURLINS MUST HAVE</td></z≤10m<>	h/d ≤ 0.5	All	535	535	TIMBER PURLINS MUST HAVE			
				h/d > 0.5 h/d ≤ 0.5	All	545 480	545 480	TIMBER PURLINS MUST HAV			
			10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>489</td><td>489</td><td> FASTENERS FIXED TO COLD </td></z≤15m<>	h/d > 0.5	All	489	489	 FASTENERS FIXED TO COLD 			
			15m <z≤20m< td=""><td>h/d ≤ 0.5 h/d > 0.5</td><td>All</td><td>442</td><td>442</td><td>DIAMETER OF THE SCREW.</td></z≤20m<>	h/d ≤ 0.5 h/d > 0.5	All	442	442	DIAMETER OF THE SCREW.			
			2000 4742000	h/d ≤ 0.5	All	450 401	450 401	 STEEL PURLINS MUST HAVE 			
		10≤α≤30	20m <z≤30m< td=""><td>h/d > 0.5</td><td>All</td><td>408</td><td>408</td><td>STEEL PURLINS MUST HAVE</td></z≤30m<>	h/d > 0.5	All	408	408	STEEL PURLINS MUST HAVE			
			0≤z≤5m	h/d ≤ 0.5 h/d > 0.5	All	516 543	516 543	PARTRIDGE ENGINEERS Pty			
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>460</td><td>460</td><td>USE BY SCHLETTER AUSTRINSTALLATION VERIFICATIO</td></z≤10m<>	h/d ≤ 0.5	All	460	460	USE BY SCHLETTER AUSTRINSTALLATION VERIFICATIO			
				h/d > 0.5 h/d ≤ 0.5	All	484 413	484 413	NO ALLOWANCE HAS BEEN			
			10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>435</td><td>435</td><td>INSTALLATION OUTSIDE THIS</td></z≤15m<>	h/d > 0.5	All	435	435	INSTALLATION OUTSIDE THIS			
_			15m <z≤20m< td=""><td>h/d ≤ 0.5 h/d > 0.5</td><td>All</td><td>380 400</td><td>380 400</td><td>INSTALLATIONS IN TERRAIN</td></z≤20m<>	h/d ≤ 0.5 h/d > 0.5	All	380 400	380 400	INSTALLATIONS IN TERRAIN			
			20m <z≤30m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>344</td><td>344</td><td>FOLLOWING;</td></z≤30m<>	h/d ≤ 0.5	All	344	344	FOLLOWING;			
			2011 - 2200111	h/d > 0.5 h/d ≤ 0.5	All	363 662	363 662	Region A = 18%			
			0≤z≤5m	h/d ≥ 0.5	All	662 674	674	Region B = 18%			
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>662</td><td>662</td><td>Region C/D = Specific enginee</td></z≤10m<>	h/d ≤ 0.5	All	662	662	Region C/D = Specific enginee			
		<5°		h/d > 0.5 h/d ≤ 0.5	All	674 573	674 573	• REFER TO AS1170.2:2021 SE			
	TC3	0<5°	10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>584</td><td>584</td><td>SOLAR PANELS HAVE BEEN SOLAR PANELS HAVE BEEN</td></z≤15m<>	h/d > 0.5	All	584	584	SOLAR PANELS HAVE BEEN SOLAR PANELS HAVE BEEN			
			15m <z≤20m< td=""><td>h/d ≤ 0.5 h/d > 0.5</td><td>All</td><td>512 522</td><td>512 522</td><td>FOR THE VARIOUS SPANS A</td></z≤20m<>	h/d ≤ 0.5 h/d > 0.5	All	512 522	512 522	FOR THE VARIOUS SPANS A			
			20m <z≤30m< td=""><td>h/d > 0.5</td><td>All</td><td>451</td><td>451</td><td> ALL SPANS IN THE TABLE N ROOF. </td></z≤30m<>	h/d > 0.5	All	451	451	 ALL SPANS IN THE TABLE N ROOF. 			
			2011-235011	h/d > 0.5 h/d ≤ 0.5	All	460	460				
		5≤α<10°	0≤z≤5m	h/d ≥ 0.5	All	662 674	662 674	REDUCTION FAC			
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>662</td><td>662</td><td>FASTENERS</td></z≤10m<>	h/d ≤ 0.5	All	662	662	FASTENERS			
				h/d > 0.5 h/d ≤ 0.5	All	674 573	674 573	IASTENERS			
			10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>584</td><td>584</td><td>SPANS FROM THE ABOVE TABL</td></z≤15m<>	h/d > 0.5	All	584	584	SPANS FROM THE ABOVE TABL			
			15m <z≤20m< td=""><td>h/d ≤ 0.5 h/d > 0.5</td><td>All</td><td>512 522</td><td>512 522</td><td>THAN 4 A-FRAMES. WHERE A R</td></z≤20m<>	h/d ≤ 0.5 h/d > 0.5	All	512 522	512 522	THAN 4 A-FRAMES. WHERE A R			
			20m <z<20m< td=""><td>h/d > 0.5</td><td>All</td><td>451</td><td>451</td><td>SHOULD BE MULTIPLIED BY TH</td></z<20m<>	h/d > 0.5	All	451	451	SHOULD BE MULTIPLIED BY TH			
		10≤α≤30	20m <z≤30m< td=""><td>h/d > 0.5</td><td>All</td><td>460</td><td>460</td><td></td></z≤30m<>	h/d > 0.5	All	460	460				
			0≤z≤5m	h/d ≤ 0.5 h/d > 0.5	All	568 599	568 599	RAIL SUPPORT REDUCTION FA			
			5m <z≤10m< td=""><td>h/d ≤ 0.5</td><td>All</td><td>568</td><td>568</td><td>NOTE: RAIL MUST SPAN BETWE</td></z≤10m<>	h/d ≤ 0.5	All	568	568	NOTE: RAIL MUST SPAN BETWE			
				h/d > 0.5 h/d ≤ 0.5	All	599 492	599 492	INOTE. NAIL WOST SPAN BETWE			
			10m <z≤15m< td=""><td>h/d > 0.5</td><td>All</td><td>519</td><td>519</td><td></td></z≤15m<>	h/d > 0.5	All	519	519				
			15m <z≤20m< td=""><td>h/d ≤ 0.5 h/d > 0.5</td><td>All</td><td>440 464</td><td>440</td><td></td></z≤20m<>	h/d ≤ 0.5 h/d > 0.5	All	440 464	440				
			20m <z≤30m< td=""><td>h/d > 0.5</td><td>All</td><td>388</td><td>464 388</td><td>1</td></z≤30m<>	h/d > 0.5	All	388	464 388	1			
				h/d > 0.5							

A Frame 30 Degree Tilt - Fixing to substructure - F7 Softwood - Using Using 2/Bremick Vortex

Universal Screw - 2100 Modules

DESIGN PARAMETERS

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WIND PARAMETERS ARE IN ACCORDANCE WITH AS/NZS1170.2:2021. EARTHQUAKE AND SNOW LOADS ARE EXCLUDED TABLES ARE SUITABLE FOR BUILDINGS INCLUSIVE OF PARAMETERS REFFERED TO IN THE TABLES BELOW AND ASSUMPTION MANUAL ATTACHED. REGION = A, B, C, D

Base Wind Speed

Region | A | B | C | D Vr(m/s) | 43 | 52 | 61 | 72

GENERAL

SPAN TABLE TO BE READ WITH PARTRIDGE ASSUMPTIONS MANUAL

- REVIEW OF SUPPORTING BUILDING FOR STRUCTURAL ADEQUACY TO SUPPORT PANEL INSTALLATION BY OTHERS.
- REVIEW OF ROOF SHEETING FOR STRUCTURAL ADEQUACY TO SUPPORT PANEL INSALLATION BY OTHERS.
- THESE SPANS ARE ONLY APPLICABLE TO CONTINUOUS RAILS SUPPORTED BY A MINIMUM OF 4 A-FRAMES. SEE BELOW FOR SPAN REDUCTION FACTORS FOR RAILS SUPPORTED BY LESS THAN 4 A-FRAMES.
- REVIEW OF SOLAR PANEL STRUCTURAL CAPACITY BY OTHERS.
- A-FRAMES TO BE FIXED TO THE SUB STRUCTURE OR ROOF SHEETING WITH THE QUANTITY AND TYPE OF SCREWS NOTED IN THE TABLE.
- ALL FIXTURES TO BE INSTALLED TO THE MANUFACTURERS SPECIFICATIONS.
- ALLOWANCE HAS BEEN MADE FOR A SOLAR PANEL SELF WEIGHT OF 0.15 kPa.
- 2 RAILS MINIMUM ARE TO BE USED FOR ALL WIND REGIONS. RAILS TO BE LOCATED 15%-25% OF THE PANELS
- LENGTH FROM THE EDGE. PANELS TO BE ORIENTATED IN THE PORTRAIT POSITION.
- ALL RAILS ARE TO BE JOINED WITH RAIL CONNECTORS DOCUMENTED IN SCHLETTER Pty Ltd TECHNICAL ARTICLE
- ALL RAILS TO SPAN THREE FULL SPAN MINIMUM (BE SUPPORTED BY MIN 4 FASTENERS). CANTILEVERS TO BE A MAXIMUM OF 40% OF THE ADJACENT SPAN CAPACITY.
- ALL RAILS, CLAMPS AND FASTENERS TO BE INSTALLED IN ACCORDANCE WITH THEIR RELEVANT SCHLETTER INC.
- DOCUMENTATION. FASTENERS FIXED TO TIMBER MUST HAVE AN EDGE DISTANCE OF 5D, WHERE 'D' IS THE DIAMETER OF THE SCREW.
- THIS IS IN COMPLIANCE WITH EDGE DISTANCES OUTLINED IN AS1720.1:2010 SECTION 4.3.4.
- FASTENERS FIXED TO TIMBER FRAMING MUST USE A BREMICK VORTEX UNIVERSAL SCREW, WITH MINIMUM DIAMETER OF 6.2mm, AND A MINIMUM EMBEDMENT OF 35mm.
- TIMBER PURLINS MUST HAVE A MINIMUM WIDTH OF 10D WHERE D IS THE DIAMETER OF THE TIMBER SCREW.
- TIMBER PURLINS MUST HAVE A MINIMUM GRADE OF F7 AS DEFINED IN AS1720.1.
- FASTENERS FIXED TO COLD FORMED STEEL PURLINS MUST HAVE AN EDGE DISTANCE OF 3D WHERE 'D' IS THE DIAMETER OF THE SCREW. THIS IS IN COMPLIANCE WITH EDGE DISTANCES OUTLINED IN AS4600:2-18 SECTION 5.4.3
- STEEL PURLINS MUST HAVE A MINIMUM BASE METAL EQUAL TO THE VALUE SPECIFIED IN THE TABLE.
- STEEL PURLINS MUST HAVE A MINIMUM WITDTH OF 6D WHERE D IS THE DIAMETER OF THE STEEL SCREW. PARTRIDGE ENGINEERS Pty Ltd PREPARED DOCUMENTATION, PROJECT NUMBER 2021S0925, IS FOR THE EXCLUSIVE
- USE BY SCHLETTER AUSTRALIA PTY LTD ONLY.
- INSTALLATION VERIFICATION AND ASSOCIATED CERTIFICATION IS BY OTHERS. NO ALLOWANCE HAS BEEN MADE FOR HYDRAULIC, HAIL OR SNOW LOADING.
- INSTALLATION OUTSIDE THE SPECIFIC PARAMETERS REQUIRES SPECIFIC ENGINEERING ANALYSIS.
- INSTALLATIONS IN TERRAIN CATEGORY = 1.0, REDUCE EQUIVALENT TERRAIN CATEGORY 2.0 VALUES BY THE
- FOLLOWING; Region A = 18%
- Region B = 18%
- Region C/D = Specific engineering review required.
- REFER TO AS1170.2:2021 SECTION 4.2.1 FOR THE DETERMINATION OF TERRAIN CATEGORY.
- SOLAR PANELS HAVE BEEN CHECKED FOR WIND LOADINGS AND SHOULD BE CERTIFIED BY THE MANUFACTURER
- FOR THE VARIOUS SPANS AND WIND REGIONS. ALL SPANS IN THE TABLE MUST BE MULTIPLIED BY A REDUCTION FACTOR BASED ON THEIR POSITION ON THE

REDUCTION FACTORS FOR RAILS SUPPORTED BY LESS THAN 4 FASTENERS

SPANS FROM THE ABOVE TABLE CANNOT BE USED ON CONTINUOUS RAILS THAT ARE SUPPORTED BY LESS THAN 4 A-FRAMES. WHERE A RAIL IS SUPPORTED BY LESS THAN 4 A-FRAMES THE SPANS IN THE TABLE SHOULD BE MULTIPLIED BY THE BELOW FACTOR.

RAIL SUPPORT REDUCTION FACTOR = 0.89

NOTE: RAIL MUST SPAN BETWEEN MIN TWO FASTENERS

REDUCTION FACTOR FOR SOLAR PANEL LOCATION ON

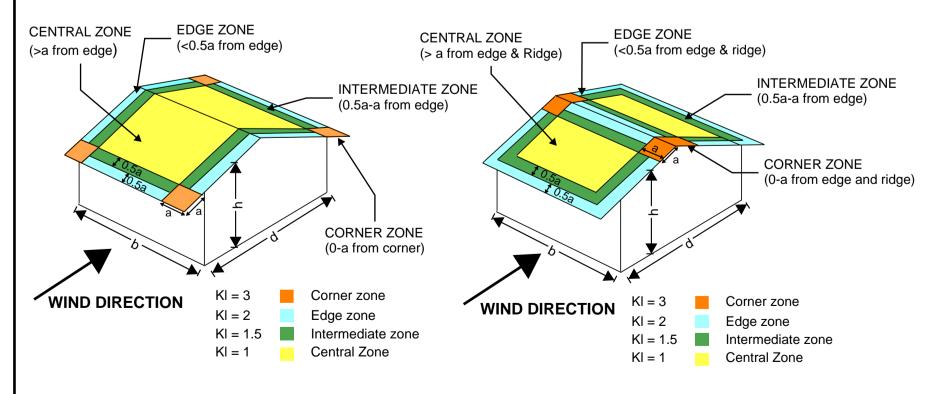
ALL A-FRAME SPACINGS IN THE ABOVE TABLE MUST BE MULTIPLIED BY ONE OF THE BELOW FACTORS BASED ON THEIR LOCATION ON THE ROOF.

CORNER ZONE: SPACINGS MUST BE MULTIPLIED BY 0.33 EDGE ZONE: SPACINGS MUST BE MULTIPLIED BY 0.5 INTERMEDIATE ZONE: SPACINGS MUST BE MULTIPLIED BY 0.66

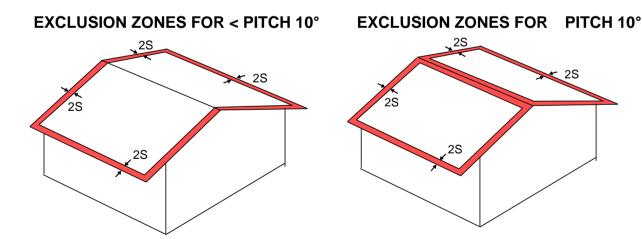
CENTRAL ZONE: SPACINGS DO NOT NEED TO BE MULTIPLIED BY ANY FACTOR

WHERE a = MIN(0.2d, 0.2b) if h/d or h/b 0.2, or 2h if h/d and h/b < 0.2 ROOF ZONES FOR ROOVES WITH PITCHES < 10°

ROOF ZONE FOR ROOVES WITH PITCHES 10°



SOLAR PANEL EXCLUSION ZONE & MOUNTING RESTRAINTS



PANELS MUST NOT BE INSTALLED WITHIN A DISTANCE OF 2S FROM THE ROOF EDGE WHERE S IS THE GAP BETWEEN THE UNDERSIDE OF THE PANEL AND THE ROOF SURFACE (ROOF EDGE INCLUDES RIDGES WITH PITCH 10)

THE EXCLUSION ZONE SHOWN ABOVE MUST BE MIN 200mm.

THE GAP BETWEEN THE UNDERSIDE OF THE PANEL AND THE ROOF SURFACE MUST BE MIN 50mm AND MAX 300mm

TERRAIN CATEGORY DEFINITIONS

AS1170.2 :2021 CLAUSE 4.2.1

TC1 - VERY EXPOSED OPEN TERRAIN WITH VERY FEW OR NO OBSTRUCTIONS, AND ALL WATER SURFACES

TC2 - OPEN TERRAIN, INCLUDING GRASSLAND, WITH WELL SCATTER OBSTRUCTIONS HAVING HEIGHTS GENERALLY FROM 1.5m TO 5m, WITH NO MORE THAN TWO OBSTRUCTIONS PER HECTARE

TC2.5 - TERRAIN WITH SOME TREES OR ISOLATED OBSTRUCTIONS, TERRAIN IN DEVELOPING OUTER URBAN AREAS WITH SCATTERED HOUSES, OR LARGE ACREAGE DEVELOPMENTS WITH MORE THAN TWO AND LESS THAN 10 BUILDINGS PER HECTARE

TC3 - TERRAIN WITH NUMEROUS CLOSELY SPACED OBSTRUCTIONS HAVING HEIGHTS GENERALLY FROM 3m TO 10m. THE MINIMUM DENSITY OF OBSTRUCTIONS SHALL BE ATLEAST THE EQUIVALENT OF 10 HOUSE-SIZE OBSTRUCTIONS PER HECTARE

TC4 - TERRAIN WITH NUMEROUS LARGE, HIGH (10m TO 30m TALL) AND CLOSELY SPACED CONSTRUCTIONS, SUCH AS LARGE CITY CENTRES AND WELL-DEVELOPED INDUSTRIAL COMPELXES.

ALTERATIONS TO SPAN TABLES FOR SOLAR PANEL SIZE

THIS SPAN TABLE IS FOR SOLAR PANELS OF SIZE 2100x1100mm, EACH RAIL SUPPORTS A SOLAR PANEL WIDTH OF 1050mm. THE SPACINGS SHOWN IN THE TABLES HAVE BEEN CALCULATED ASSUMING EACH PANEL IS SUPPORTED WITH TWO RAILS. THE SPANS IN THE TABLE CAN BE ALTERED FOR LARGER & SMALLER SOLAR PANELS USING THE FOLLOWING EQUATIONS.

FOR SOLAR PANELS WITH WIDTH LARGER THAN 2100mm

$$Span * \frac{2100}{y}$$

Where y = NEW SOLAR PANEL WIDTH IN mm

FOR SOLAR PANELS WITH WIDTH SMALLER THAN 2100mm

$$Span * \sqrt{\frac{2100}{y}}$$

WHERE y = NEW SOLAR PANEL WIDTH IN mm

ALTERATIONS TO SPAN TABLES FOR ADDITIONAL RAILS

THIS SPAN TABLE IS FOR SOLAR PANELS OF SIZE 2100x1100mm. EACH RAIL SUPPORTS A SOLAR PANEL WIDTH OF 1050mm. THE SPACINGS SHOWN IN THE TABLES HAVE BEEN CALCULATED ASSUMING EACH PANEL IS SUPPORTED WITH TWO RAILS. THE SPANS IN THE TABLE CAN BE ALTERED FOR ADDITIONAL RAILS USING THE FOLLOWING EQUATION.

$$Span * \sqrt{\frac{1050}{\left(\frac{2100}{n}\right)^2}}$$

WHERE n = THE TOTAL NUMBER RAILS SUPPORTING THE PANEL. RAILS MUST BE SPACED SO THAT THEY SUPPORT EVEN WIDTHS OF THE PANEL

A FOR INFORMATION JW AKD 4/10/2023 By App. Date Rev Issue / Amendment



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SCHLETTER AUSTRALIA PTY LTD

2021S0925

A FRAME 30 DEGREE SETUP FIXING TO F7 SOFTWOOD USING 2/BREMICK VOTREX UNIVERSAL SCREWS

2100 MODULES

ELECTRONIC SIGNATURE: THIS DRAWING HAS BEEN ASSIGNED AN ELECTRONIC SIGNATURE DO NOT SCALE DRAWINGS CODE. THE PRESENCE OF THIS CODE SIGNIFIES THAT THIS IS THE USE FIGURED DIMENSIONS CERTIFIED DRAWING ISSUED FOR CONSTRUCTION. Electronic Code Signature Date Designed JW Scale at A1 Drawn

04/10/2023 JW Job No. Drawing No. Revision 2021S0925